LOGAN'S LANDING

Woodland, WA

TRAFFIC IMPACT ANALYSIS (TIA) July 31, 2023



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1. INTRODUCTION

The main goals of this study focus on the assessment of existing roadway conditions and forecasts of newly generated project traffic. The first task includes the review of general roadway information on the adjacent street system and baseline vehicular volumes. Forecasts of future traffic and dispersion patterns on the street system are then determined using established trip generation and distribution techniques. As a final step, appropriate conclusions and mitigation measures are defined if needed.

2. PROJECT DESCRIPTION

Logan's Landing is a proposed mixed-use development located within the city of Woodland. The subject site is located west of Old Pacific Highway and south of Belmont Loop. The subject site, comprised of four parcels (#: 50680023, 50714, 50729 and a portion of 50730), is situated on approximately 20 acres of undeveloped land. Development is proposed to consist of eight buildings, each with 5,080 square feet of office/retail space on the bottom floor (40,640 square feet total) and the top floors will consist of a total of 34 apartments units (272 total units on-site). Access to and from the subject site is proposed via a southerly extension of Franklin Street by way of Belmont Loop. Moreover, this Franklin Street roadway extension is proposed to provide direct connection to Old Pacific Highway via parcel #: 50714 upon full site build-out. Figure 1 below depicts the roadway network servicing the subject site. Figure 2 on the following page highlights the site layout.







3. EXISTING CONDITIONS

3.1 Existing Street System

The street network serving the proposed project consists of a variety of roadways. The major roadways and arterials surrounding the site are listed and described in Table 1 below.

| Functional Classification | Roadway | Speed Travel Limit Lanes I | | Street Parking | Sidewalk | Bike Facilities | | | | | | | |
|------------------------------|-----------------|-------------------------------|---|-------------------|---------------|--------------------|--|--|--|--|--|--|--|
| | Dike Access Rd | 35-mph | 2 | No | Discontinuous | No | | | | | | | |
| Minor Arterial | Old Pacific Hwy | 35-mph | 2 | No | Discontinuous | No | | | | | | | |
| | Lewis River Rd | 35-mph | 2 | No | Discontinuous | No | | | | | | | |
| Local | Belmont Loop | 25-mph* | 2 | Yes | Discontinuous | No | | | | | | | |

Table 1: Roadway Network

* No posted speed limit observed so 25 mph assumed.

3.2 Transit Service

No transit is available within walking-distance of the subject site. The nearest public transit is provided at the Woodland Park & Ride, located ~1.5-miles south of the subject site. The Lower Columbia CAP (Community Action Program) provides weekday transit service from Longview to Vancouver, with stops in Woodland and Kalama. Service is available from 6:35 AM – 6:28 PM with approximately 120-minute headways. Refer to the CAP schedule for more detailed information.

Given the proximity of the Woodland Park & Ride to the proposed development, residents may utilize transit services.

3.3 Non-Motorist Infrastructure

Discontinuous segments of sidewalk are available along Belmont Loop, adjacent developed tax parcels. The surrounding area, including Old Pacific Highway, is rural in nature with minimal non-motorist infrastructure available. The Franklin Street roadway extension will be constructed as part of site development, providing sidewalk infrastructure.



3.4 Roadway Improvements

A review of the City of Woodland's Six-Year Transportation Improvement Program (2023-2028) indicates that the following projects are currently planned in the vicinity of Logan's Landing development.

| Table 2: Transportation Improvement Projects | | | | | | | | | | | |
|---|---|--|--------------|--|--|--|--|--|--|--|--|
| Name | Location | Improvement | Cost | | | | | | | | |
| SR 503 Bypass (WA-11289) | Lewis River Rd to OPH | Construct a new roadway to bypass SR 503 extending from Lewis River Rd to OPH thereby providing a more direct route with access via I- 5/Dike Access Rd | TBD | | | | | | | | |
| OPH Sidewalks (WA-14418) | OPH: Belmont Loop to E Scott | Install sidewalks and ADA ramps along roadway | TBD | | | | | | | | |
| Hillsdale OPH Ext. (WA-11272) | OPH to Green Mtn. | Extend Hillsdale Dr from its current terminus point at Green Mtn Rd easterly to OPH (roughly mid-point btw Belmont Lp N and S). Phase 1 is expected to begin in 2026. Project cost/funding status are TBD. | TBD | | | | | | | | |
| Green Mt./OPH (WA-11271) | Intersection | Construct intersection improvements | TBD | | | | | | | | |
| Franklin Loop/OPH (WA-11269) | Franklin Loop | Extend Franklin southerly from its current terminus point ~275' s/o Belmont, jogging easterly to tie into OPH at Woodland View. A portion of this project would be constructed as part of Logan's Landing. | TBD | | | | | | | | |
| Franklin/E Scott Ext. (WA-11270) | Franklin Loop | Extend Franklin southerly from the above project to E Scott. Phase 1 is expected to commence in 2027. Project cost/funding status are TBD. | TBD | | | | | | | | |
| E Scott/OPH (WA-05177) | Intersection | Construct intersection improvements. Final design is TBD. | \$3,200,000 | | | | | | | | |
| W Scott Ave Full Depth Reclamation (WA-05176) | W. Scott Ave: Schurman Way to Pac. Ave. | Full depth reclamation and sidewalks. Project will coordinate with separately funded Pedestrian and Water line RR crossing projects. | \$2,207,996 | | | | | | | | |
| SR-503 Safety Project (WA-12751) | N Goerig to Gun Club Rd | Install sidewalk, planter strips, curb & gutter, bike route, crosswalk w/ signage & RRFBs | \$1,514,080 | | | | | | | | |
| W Scott/Pacific Slip Lane (WA -11286) | W Scott/Pacific | Construct a slip lane | TBD | | | | | | | | |
| Scott Hill Connectors (WA-11288) | Scott Hill | Provide roadway connections between Meriwether and Scott Hill | TBD | | | | | | | | |
| Scott Ave Reconnection (WA-06621) | Scott Ave | Engineering, design, and construction of Scott Avenue crossing at I-5 | \$81,000,000 | | | | | | | | |



3.5 Existing Peak Hour Volumes

Field data for this study was obtained and collected by our firm in June of 2023 at the following study intersections:

- 1. Dike Access Road & I-5 Southbound Ramps
- 2. Dike Access Road & I-5 Northbound Ramps
- 3. Old Pacific Highway & Belmont Loop N
- 4. Old Pacific Highway & Belmont Loop S
- 5. Old Pacific Highway & Green Mountain Road
- 6. Old Pacific Highway & E Scott Avenue
- 7. Lewis River Road & E Scott Avenue

Counts were performed between the PM peak period of 4:00 PM - 6:00 PM, which generally represents peak roadway conditions during a typical 24-hour period. The single hour exhibiting highest overall intersection volumes is then derived (peak hour) and is used for analysis for each respective location. Figure 3 on the following page identifies baseline PM peak hour volumes. Full count sheets have been attached in the appendix for reference.

It should be noted that the prior *Logan's Landing TIA (3/10/2022)* derived baseline PM peak hour volumes consistent with methodologies utilized in the *Oak Village Apartments TIA (8/19/2021)* by Lancaster Mobley. Traffic patterns and volumes were presumably depressed by the ongoing COVID-19 pandemic at the time both reports were conducted. As such, baseline intersection volumes were established by grossing up historic 2019 pre-COVID counts by a compound annual growth rate of 2.3 percent, as well as by adjusting up 2021 counts by a derived factor of 1.3881. However, as traffic conditions are presumed to now have stabilized in 2023, all new counts have been gathered, which are anticipated to accurately reflect baseline conditions. This is corroborated by 2023 total intersection volumes gathered by our firm at the Dike Access Road I-5 Ramps, which comprise similar travel patterns and volumes to pre-COVID counts utilized for the *Oak Village Apartments TIA*.

Lastly, non-motorist volumes were observed at the Old Pacific Highway intersections located in closest proximity to the subject site. No pedestrians or bicycle transport were observed along Old Pacific Highway at Belmont Loop (North or South) or at Green Mountain Road. Given the rural nature of surrounding development, the subject site is not anticipated to be a significant generator of non-motorist traffic.







3.6 Level of Service

Existing intersection delays were determined through the use of the *Highway Capacity Manual* 7th Edition. Capacity analysis is used to determine level of service (LOS) which is an established measure of congestion for transportation facilities. The range¹ for intersection level of service is LOS A to LOS F with the former indicating the best operating conditions with low control delays and the latter indicating the worst conditions with heavy control delays. Detailed descriptions of intersection LOS are given in the 2016 Highway Capacity Manual. Level of service calculations were made through the use of the *Synchro 12* and *SIDRA 9.1* analysis programs. For roundabouts and all-way stop-controlled (AWSC) intersections, LOS is determined by the intersection's overall weighted average delay for each approaching leg. Sidestreet stop-controlled intersection LOS is determined by the approach with the highest delay. Table 3 presents existing PM peak hour LOS delays for the key intersections of study.

| Intersection | Control | Movement | LOS | Delay |
|----------------------------------|---------|----------|-----|-------|
| I-5 SB Ramps & Dike Access Rd | RAB | Overall | А | 7.6 |
| I-5 NB Ramps & Dike Access Rd | RAB | Overall | А | 8.2 |
| Belmont Loop N & Old Pacific Hwy | TWSC | EB | С | 16.32 |
| Belmont Loop S & Old Pacific Hwy | TWSC | EB | В | 12.96 |
| Green Mtn Rd & Old Pacific Hwy | TWSC | WB | В | 12.67 |
| E Scott Ave & Old Pacific Hwy | AWSC | Overall | В | 11.6 |
| E Scott Ave & Lewis River Rd | RAB | Overall | А | 6.9 |

| Table 3: Existing | Weekday PM Peak Hour Level of Service |
|-------------------|---------------------------------------|
| | |

The City of Woodland has adopted LOS D standards. Existing PM peak hour conditions at the study intersections are shown to operate with delays at LOS C or better. As such, the study intersections meet City standards under existing conditions.

| ¹ Signalized Intersections - Level of Service | | | | | | | | | |
|--|----------------------|--|--|--|--|--|--|--|--|
| Control Delay pe | r | | | | | | | | |
| Level of Service | <u>Vehicle (sec)</u> | | | | | | | | |
| A | ≤10 | | | | | | | | |
| В | >10 and ≤20 | | | | | | | | |
| С | >20 and ≤35 | | | | | | | | |
| D | >35 and ≤55 | | | | | | | | |
| E | >55 and ≤80 | | | | | | | | |
| F | >80 | | | | | | | | |

Highway Capacity Manual, 7th Edition



Stop Controlled Intersections - Level of Service

Vehicle (sec)

>10 and ≤15

>15 and ≤25

>25 and ≤35

> 35 and ≤ 50

≤10

>50

Control Delay per Level of Service

А

В

С

D

Е

F

4. FORECAST TRAFFIC DEMAND & ANALYSIS

4.1 Project Trip Generation

Trip generation is used to determine the magnitude of project impacts on the surrounding street system. This is usually denoted by the quantity or specific number of new trips that enter and exit a project during a designated time period, such as a specific peak hour (AM or PM) or an entire day. Data presented in this report was taken from the Institute of Transportation Engineer's publication Trip Generation, 11th Edition. It should be noted that the ground-level commercial space users are unknown at this time. The commercial space is anticipated to be split roughly half between general office and half as general retail. As such, the designated land uses for this project are defined under Land Use Code (LUC) 220 – Multi-Family (Low-Rise) Apartments (272 dwelling units), LUC 710 – General Office (20,320 square feet) and LUC 821 – Strip Retail Plaza (<40k: 20,320 square feet).

It should be noted that the proposed project is anticipated to generate trips from internal capture (i.e., customers/residents already on-site) and pass-by (i.e., customers already on the adjacent street system) in addition to new trips. Concerning internal capture, a single trip entering the site for one facility may subsequently use a variety of other services offered on-site. Moreover, residents within the multi-family space may utilize commercial/retail services on-site. The complimentary uses on-site are anticipated to generate an internal trip capture reduction of 5.1% in the AM peak hour and 21.5% in the PM peak hour as derived via the NCHRP 8-51 Internal Trip Capture Estimation Tool. Also considered are pass-by trips, or motorists already passing by the site who decide to make an intermediate stop before proceeding to their primary destination. Pass-by percentages were applied to the proposed 20,320 square feet of strip retail space on-site based on ITE data. These trips are not considered as new trips but will impact the site's access points.

Table 4 on the following page summarizes the estimated aggregate project trip generation. Included are the average weekday daily traffic (AWDT) and the AM and PM peak hours. Available in the appendix is a use-specific breakdown including rates used for calculations.



Logan's Landing TIA 11

| Trin Type | | AM P | eak-Hou | ır Trips | PM Peak-Hour Trips | | | | | | | |
|--------------------------------------|------|------|---------|----------|--------------------|-----|-------|--|--|--|--|--|
| тар туре | AWDI | In | Out | Total | In | Out | Total | | | | | |
| Total Trips | 3160 | 82 | 106 | 188 | 159 | 143 | 302 | | | | | |
| Internal Link Reduction ² | -420 | -6 | -4 | -10 | -34 | -31 | -65 | | | | | |
| Pass-By Reduction ³ | -384 | -9 | -9 | -18 | -21 | -21 | -42 | | | | | |
| Total New Primary | 2356 | 67 | 93 | 160 | 104 | 91 | 195 | | | | | |

Table 4: Project Trip Generation

As summarized in Table 4, trips to and from the site are broken into internal capture, pass-by and primary. In total, 2,356 new primary vehicular trips per weekday are expected as a result of the proposed development with 160 primary trips occurring during the AM peak hour and 195 primary trips occurring during the PM peak hour. Moreover, approximately 18 AM peak hour and 42 PM peak hour trips are anticipated to be generated from the development in the form of pass-by.

4.2 Distribution & Assignment

Trip distribution describes the anticipated travel routes for inbound and outbound project traffic during the peak hour study period. PM peak hour trips are primarily comprised of commuter-based (returning home) and recreational-based trips. Primary and pass-by PM peak hour trips generated by the project are expected to follow the general pattern as shown in Figure 4. Percentages emulate prior submittals for the Logan's Landing project. An approximate 75/25 north/south split is anticipated for both primary and pass-by trips. Trips were assigned to the Belmont Loop South & Old Pacific Highway intersection via the Franklin Street extension. Moreover, trips were additionally assigned to the newly proposed Franklin Street extension connection to Old Pacific Highway via tax parcel #: 50714.

4.3 Future Peak Hour Volumes

A three-year horizon of 2026 was used to analyze future conditions. Background volumes at the intersections of study were derived by applying a 2.3 percent compound annual growth rate to the existing volumes illustrated in Figure 3. This growth rate was derived from the City's Comprehensive Plan based on their population growth forecasts. Moreover, pipeline volumes from the Oak Village Apartments project were accounted for in forecast volumes. Figures 5 and 6 represent forecast 2026 PM peak hour volumes without and with project traffic.

³ Pass-by rates were derived from the Institute of Transportation Engineers, *2021 Pass-By Tables for ITE Trip Gen Appendices* (2021). As no pass-by data is available for LUC 822 - Strip Retail Plaza (<40k), data for LUC 821 - Shopping Plaza (40 - 150k) was utilized. PM Rate: 40%. This rate was applied to ADT and AM.



² An internal link reduction of 5.1% was applied to all proposed on-site land uses for the AM peak hour and 21.5% for the PM peak hour, which was derived via the NCHRP 8-51 Internal Trip Capture Estimation Tool. ADT internal capture rates were derived by taking the average of the AM and PM peak hours (13.3%).













4.4 Future Level of Service

Level of service analyses were made of the future PM peak hour volumes without (background) and with project related trips added to the key roadways and intersections. This analysis once again involved the use of the *Synchro 12* and *SIDRA 9.1* analysis programs. Delays for the study intersections under future conditions are shown below in Table 5.

| | | | 1 | | | | |
|---------------------------------------|---------|-----------|---------------|------------------|---------------------|-------|--|
| | | | <u>Withou</u> | <u>t Project</u> | <u>With Project</u> | | |
| Intersection | Control | Peak Hour | LOS | Delay | LOS | Delay | |
| I-5 SB Ramps & Dike Access Rd | RAB | Overall | А | 9.3 | В | 11.7 | |
| I-5 NB Ramps & Dike Access Rd | RAB | Overall | А | 9.0 | А | 9.8 | |
| Belmont Loop N & Old Pacific Hwy | TWSC | EB | С | 19.27 | С | 24.13 | |
| Belmont Loop S & Old Pacific Hwy | TWSC | EB | В | 14.13 | С | 18.89 | |
| Green Mtn Rd & Old Pacific Hwy | TWSC | WB | С | 15.01 | С | 16.11 | |
| E Scott Ave & Old Pacific Hwy | AWSC | Overall | В | 12.7 | В | 13.8 | |
| E Scott Ave & Lewis River Rd | RAB | Overall | А | 8.1 | А | 8.5 | |
| Franklin St Ext. & Old Pacific Hwy | TWSC | EB | - | - | В | 14.69 | |

 Table 5: Forecast 2026 Weekday Peak Hour Level of Service

 Delays Given in Seconds per Vehicle

Forecast 2026 weekday peak hour delays are shown to operate with up to LOS C conditions with or without the proposed development at all study intersections. As such, no level of service deficiencies are identified and all intersections meet City standards.

It should be noted that the City's Six-Year Transportation Improvement Plan has budgeted approximately \$3,200,000 for improvements at E Scott Avenue & Old Pacific Highway. While specific improvements were not identified under their current plan, conditions would likely subsequently improve by reducing delays and increasing capacity. Moreover, several City-planned projects were additionally identified within the study area that would result in improved conditions. These include intersection improvements at Old Pacific Highway & Green Mountain Road, the SR 503 Bypass project and other street connections and extensions, which are anticipated to further expand travel routes and provide relief along certain corridors.



4.5 Project Access & Sight Distance

The primary access intersections of Belmont Loop Road & Franklin Street as well as newly proposed connection of Old Pacific Highway & Franklin Street were examined in terms of available sight lines. The established city of Woodland sight distance standards for controlled intersections were utilized. With no observed posted speed on Belmont Loop, the local access roadway was assumed to comprise a 25-mph speed limit. As such, approximately 250-feet of visibility would be required for traffic departing Franklin Street entering Belmont Loop. Based on a review of the existing intersection geometry, sight lines are available to 280-feet in the east/west directions with clear visibility to Old Pacific Highway. No sight distance deficiencies are identified at the intersection.

Moreover, approximately 350 feet of entering sight distance would be required at Old Pacific Highway & Franklin Street based on the 35-mph posted speed limit. Preliminary measurements at the access intersection indicate sight lines are available north and south in excess of 500 feet. No sight distance deficiencies are identified at this time.

4.6 Left Turn Warrant Analysis

Turn lanes are a means of providing necessary storage space for left turning vehicles at intersections. For this impact study, procedures described by the WSDOT Design Manual Exhibit 1310-7a were used to ascertain storage requirements at a newly proposed roadway connection of Old Pacific Highway & Franklin Street. Based on the criteria set forth in the warrant calculations, a left turn lane *would not be warranted* under forecast 2026 PM peak hour conditions at the proposed study intersection. Turn lane exhibit sheets have been included in the appendix.



5. CONCLUSIONS & MITIGATION

Logan's Landing proposes for the development of 272 multi-family dwelling units and approximately 40,640 square feet of retail/office space within the city of Woodland. The subject site comprises approximately 20-acres within tax parcel #'s: 50680023, 50714, 50729 and a portion of 50730. Access to the subject site is proposed via a southerly extension of Franklin Street from Belmont Loop, which bisects the subject site. This extension is proposed to jog easterly, connecting to Old Pacific Highway. A conceptual site plan illustrating the overall configuration of the project and access proposal is provided in Figure 2.

Based on ITE data, the proposed development is anticipated to generate approximately 2356 average weekday daily primary trips with 160 (67 in / 93 out) AM peak hour primary trips and 195 (104 in / 91 out) PM peak hour primary trips. A level of service (LOS) analysis was performed using a three-year horizon which included a background growth rate, pipeline development and project-generated traffic added to the roadway network.

Existing and forecast level of service (LOS) at the outlying study intersections are shown operate acceptably with LOS C or better conditions, meeting City standards. The proposed development is shown to minimally impact the surrounding roadway system. Lastly, a left turn lane warrant analysis was evaluated for the newly proposed connection of Old Pacific Highway & Franklin Street. A left-turn lane was found to not be warranted at the intersection.

Based on the analysis herein, and with the city planned project, no project-specific mitigation is identified at this time.



APPENDIX



PO Box 397 Puyallup, WA 98371

Roundabout

File Name : 4855aa Site Code : 00004855 Start Date : 6/27/2023 Page No : 1

| | Groups Printed- Passenger + - Heavy | | | | | | | | | | | | | | | | |
|---------------|-------------------------------------|-------|--------|------------|-------|------|--------|------------|------------|-------------------------------|------|------------|-----------|------|------|------------|------------|
| | I-5 S On-Ramp Dike Access Rd | | | | | | | | | I-5 S Off-Ramp Dike Access Rd | | | | | | | |
| | | South | nbound | | | West | tbound | | Northbound | | | | Eastbound | | | | |
| Start Time | Right | Thru | Left | App. Total | Right | Thru | Left | App. Total | Right | Thru | Left | App. Total | Right | Thru | Left | App. Total | Int. Total |
| 04:00 PM | 55 | 1 | 47 | 103 | 0 | 73 | 14 | 87 | 0 | 0 | 0 | 0 | 66 | 127 | 0 | 193 | 383 |
| 04:15 PM | 37 | 1 | 33 | 71 | 0 | 89 | 29 | 118 | 0 | 0 | 0 | 0 | 56 | 104 | 0 | 160 | 349 |
| 04:30 PM | 50 | 1 | 35 | 86 | 0 | 88 | 29 | 117 | 0 | 0 | 0 | 0 | 62 | 139 | 0 | 201 | 404 |
| 04:45 PM | 41 | 2 | 29 | 72 | 0 | 83 | 27 | 110 | 0 | 0 | 0 | 0 | 45 | 154 | 0 | 199 | 381 |
| Total | 183 | 5 | 144 | 332 | 0 | 333 | 99 | 432 | 0 | 0 | 0 | 0 | 229 | 524 | 0 | 753 | 1517 |
| | | | | | | | | | | | | | | | | | |
| 05:00 PM | 37 | 1 | 30 | 68 | 0 | 58 | 28 | 86 | 0 | 0 | 0 | 0 | 50 | 140 | 0 | 190 | 344 |
| 05:15 PM | 43 | 0 | 40 | 83 | 0 | 69 | 21 | 90 | 0 | 0 | 0 | 0 | 48 | 127 | 0 | 175 | 348 |
| 05:30 PM | 64 | 1 | 34 | 99 | 0 | 86 | 21 | 107 | 0 | 0 | 0 | 0 | 47 | 85 | 0 | 132 | 338 |
| 05:45 PM | 50 | 1 | 26 | 77 | 0 | 60 | 22 | 82 | 0 | 0 | 0 | 0 | 45 | 80 | 0 | 125 | 284 |
| Total | 194 | 3 | 130 | 327 | 0 | 273 | 92 | 365 | 0 | 0 | 0 | 0 | 190 | 432 | 0 | 622 | 1314 |
| | | | | | | | | | | | | | | | | | |
| Grand Total | 377 | 8 | 274 | 659 | 0 | 606 | 191 | 797 | 0 | 0 | 0 | 0 | 419 | 956 | 0 | 1375 | 2831 |
| Apprch % | 57.2 | 1.2 | 41.6 | | 0 | 76 | 24 | | 0 | 0 | 0 | | 30.5 | 69.5 | 0 | | |
| Total % | 13.3 | 0.3 | 9.7 | 23.3 | 0 | 21.4 | 6.7 | 28.2 | 0 | 0 | 0 | 0 | 14.8 | 33.8 | 0 | 48.6 | |
| Passenger + | 367 | 8 | 259 | 634 | 0 | 584 | 181 | 765 | 0 | 0 | 0 | 0 | 405 | 942 | 0 | 1347 | 2746 |
| % Passenger + | 97.3 | 100 | 94.5 | 96.2 | 0 | 96.4 | 94.8 | 96 | 0 | 0 | 0 | 0 | 96.7 | 98.5 | 0 | 98 | 97 |
| Heavy | 10 | 0 | 15 | 25 | 0 | 22 | 10 | 32 | 0 | 0 | 0 | 0 | 14 | 14 | 0 | 28 | 85 |
| % Heavy | 2.7 | 0 | 5.5 | 3.8 | 0 | 3.6 | 5.2 | 4 | 0 | 0 | 0 | 0 | 3.3 | 1.5 | 0 | 2 | 3 |

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File Name : 4855aa Site Code : 00004855 Start Date : 6/27/2023 Page No : 2

| | | I-5 S O | n-Ram | р | Dike Access Rd | | | | I-5 S Off-Ramp | | | | Dike Access Rd | | | | |
|--|-----------|---------|---------|------------|----------------|------|-------|------------|----------------|------|------|------------|----------------|------|------|------------|------------|
| | | South | bound | | | West | bound | | Northbound | | | | Eastbound | | | | |
| Start Time | Right | Thru | Left | App. Total | Right | Thru | Left | App. Total | Right | Thru | Left | App. Total | Right | Thru | Left | App. Total | Int. Total |
| Peak Hour Analysis From 04:00 PM to 05:45 PM - Peak 1 of 1 | | | | | | | | | | | | | | | | | |
| Peak Hour for | Entire In | ntersec | tion Be | gins at 04 | 4:00 PM | | | | | | | | | | | | |
| 04:00 PM | 55 | 1 | 47 | 103 | 0 | 73 | 14 | 87 | 0 | 0 | 0 | 0 | 66 | 127 | 0 | 193 | 383 |
| 04:15 PM | 37 | 1 | 33 | 71 | 0 | 89 | 29 | 118 | 0 | 0 | 0 | 0 | 56 | 104 | 0 | 160 | 349 |
| 04:30 PM | 50 | 1 | 35 | 86 | 0 | 88 | 29 | 117 | 0 | 0 | 0 | 0 | 62 | 139 | 0 | 201 | 404 |
| 04:45 PM | 41 | 2 | 29 | 72 | 0 | 83 | 27 | 110 | 0 | 0 | 0 | 0 | 45 | 154 | 0 | 199 | 381 |
| Total Volume | 183 | 5 | 144 | 332 | 0 | 333 | 99 | 432 | 0 | 0 | 0 | 0 | 229 | 524 | 0 | 753 | 1517 |
| % App. Total | 55.1 | 1.5 | 43.4 | | 0 | 77.1 | 22.9 | | 0 | 0 | 0 | | 30.4 | 69.6 | 0 | | |
| PHF | .832 | .625 | .766 | .806 | .000 | .935 | .853 | .915 | .000 | .000 | .000 | .000 | .867 | .851 | .000 | .937 | .939 |
| Passenger + | 177 | 5 | 130 | 312 | 0 | 322 | 94 | 416 | 0 | 0 | 0 | 0 | 223 | 519 | 0 | 742 | 1470 |
| % Passenger + | 96.7 | 100 | 90.3 | 94.0 | 0 | 96.7 | 94.9 | 96.3 | 0 | 0 | 0 | 0 | 97.4 | 99.0 | 0 | 98.5 | 96.9 |
| Heavy | 6 | 0 | 14 | 20 | 0 | 11 | 5 | 16 | 0 | 0 | 0 | 0 | 6 | 5 | 0 | 11 | 47 |
| % Heavy | 3.3 | 0 | 9.7 | 6.0 | 0 | 3.3 | 5.1 | 3.7 | 0 | 0 | 0 | 0 | 2.6 | 1.0 | 0 | 1.5 | 3.1 |



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Roundabout

File Name : 4855ab Site Code : 00004855 Start Date : 6/27/2023 Page No : 1

| | | | | | | Grou | ıps Prir | ited- Pas | senger | + - Hea | vy | | _ | | | | |
|---------------|-------|---------|-------|------------|-------|--------|----------|------------|--------|---------|---------|------------|-------|---------|---------|------------|------------|
| | | I-5 N O | n-Ram | р | | Old Pa | cific Hv | vy | | I-5 N C |)ff-Ram | ιp | | Dike Ad | ccess F | Rd | |
| | | South | bound | | | West | bound | | | North | nbound | | | East | bound | | |
| Start Time | Right | Thru | Left | App. Total | Right | Thru | Left | App. Total | Right | Thru | Left | App. Total | Right | Thru | Left | App. Total | Int. Total |
| 04:00 PM | 0 | 0 | 0 | 0 | 26 | 45 | 0 | 71 | 13 | 0 | 47 | 60 | 0 | 97 | 82 | 179 | 310 |
| 04:15 PM | 0 | 0 | 0 | 0 | 26 | 64 | 0 | 90 | 14 | 0 | 55 | 69 | 0 | 82 | 46 | 128 | 287 |
| 04:30 PM | 0 | 0 | 0 | 0 | 19 | 62 | 0 | 81 | 18 | 0 | 50 | 68 | 0 | 108 | 70 | 178 | 327 |
| 04:45 PM | 0 | 0 | 0 | 0 | 15 | 56 | 0 | 71 | 15 | 0 | 52 | 67 | 0 | 126 | 81 | 207 | 345 |
| Total | 0 | 0 | 0 | 0 | 86 | 227 | 0 | 313 | 60 | 0 | 204 | 264 | 0 | 413 | 279 | 692 | 1269 |
| | | | | | | | | | | | | | | | | | |
| 05:00 PM | 0 | 0 | 0 | 0 | 23 | 48 | 0 | 71 | 14 | 0 | 44 | 58 | 0 | 101 | 78 | 179 | 308 |
| 05:15 PM | 0 | 0 | 0 | 0 | 14 | 42 | 0 | 56 | 21 | 0 | 51 | 72 | 0 | 123 | 62 | 185 | 313 |
| 05:30 PM | 0 | 0 | 0 | 0 | 12 | 53 | 0 | 65 | 18 | 0 | 52 | 70 | 0 | 91 | 42 | 133 | 268 |
| 05:45 PM | 0 | 0 | 0 | 0 | 18 | 47 | 0 | 65 | 7 | 0 | 40 | 47 | 0 | 76 | 42 | 118 | 230 |
| Total | 0 | 0 | 0 | 0 | 67 | 190 | 0 | 257 | 60 | 0 | 187 | 247 | 0 | 391 | 224 | 615 | 1119 |
| | | | | | | | | | | | | | | | | | 1 |
| Grand Total | 0 | 0 | 0 | 0 | 153 | 417 | 0 | 570 | 120 | 0 | 391 | 511 | 0 | 804 | 503 | 1307 | 2388 |
| Apprch % | 0 | 0 | 0 | | 26.8 | 73.2 | 0 | | 23.5 | 0 | 76.5 | | 0 | 61.5 | 38.5 | | |
| Total % | 0 | 0 | 0 | 0 | 6.4 | 17.5 | 0 | 23.9 | 5 | 0 | 16.4 | 21.4 | 0 | 33.7 | 21.1 | 54.7 | |
| Passenger + | 0 | 0 | 0 | 0 | 143 | 403 | 0 | 546 | 114 | 0 | 373 | 487 | 0 | 780 | 490 | 1270 | 2303 |
| % Passenger + | 0 | 0 | 0 | 0 | 93.5 | 96.6 | 0 | 95.8 | 95 | 0 | 95.4 | 95.3 | 0 | 97 | 97.4 | 97.2 | 96.4 |
| Heavy | 0 | 0 | 0 | 0 | 10 | 14 | 0 | 24 | 6 | 0 | 18 | 24 | 0 | 24 | 13 | 37 | 85 |
| % Heavy | 0 | 0 | 0 | 0 | 6.5 | 3.4 | 0 | 4.2 | 5 | 0 | 4.6 | 4.7 | 0 | 3 | 2.6 | 2.8 | 3.6 |
| - | | | | | | | | | | | | | | | | | |

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File Name : 4855ab Site Code : 00004855 Start Date : 6/27/2023 Page No : 2

| | | I-5 N O | n-Ramp |) | | Old Pad | cific Hw | 'Y | | I-5 N O | ff-Ram | р | | Dike Ad | cess F | ۲d | |
|---------------|-----------|----------|----------|------------|---------|----------|----------|------------|-------|---------|--------|------------|-------|---------|--------|------------|------------|
| | | South | bound | | | West | bound | - | | North | bound | | | East | bound | | |
| Start Time | Right | Thru | Left | App. Total | Right | Thru | Left | App. Total | Right | Thru | Left | App. Total | Right | Thru | Left | App. Total | Int. Total |
| Peak Hour Ana | alysis Fi | rom 04: | 00 PM 1 | to 05:45 | PM - Pe | eak 1 of | 1 | | | | | | | | | | |
| Peak Hour for | Entire I | ntersect | tion Beg | gins at 04 | 1:30 PM | | | | | | | | | | | | |
| 04:30 PM | 0 | 0 | 0 | 0 | 19 | 62 | 0 | 81 | 18 | 0 | 50 | 68 | 0 | 108 | 70 | 178 | 327 |
| 04:45 PM | 0 | 0 | 0 | 0 | 15 | 56 | 0 | 71 | 15 | 0 | 52 | 67 | 0 | 126 | 81 | 207 | 345 |
| 05:00 PM | 0 | 0 | 0 | 0 | 23 | 48 | 0 | 71 | 14 | 0 | 44 | 58 | 0 | 101 | 78 | 179 | 308 |
| 05:15 PM | 0 | 0 | 0 | 0 | 14 | 42 | 0 | 56 | 21 | 0 | 51 | 72 | 0 | 123 | 62 | 185 | 313 |
| Total Volume | 0 | 0 | 0 | 0 | 71 | 208 | 0 | 279 | 68 | 0 | 197 | 265 | 0 | 458 | 291 | 749 | 1293 |
| % App. Total | 0 | 0 | 0 | | 25.4 | 74.6 | 0 | | 25.7 | 0 | 74.3 | | 0 | 61.1 | 38.9 | | |
| PHF | .000 | .000 | .000 | .000 | .772 | .839 | .000 | .861 | .810 | .000 | .947 | .920 | .000 | .909 | .898 | .905 | .937 |
| Passenger + | 0 | 0 | 0 | 0 | 67 | 200 | 0 | 267 | 65 | 0 | 186 | 251 | 0 | 445 | 282 | 727 | 1245 |
| % Passenger + | 0 | 0 | 0 | 0 | 94.4 | 96.2 | 0 | 95.7 | 95.6 | 0 | 94.4 | 94.7 | 0 | 97.2 | 96.9 | 97.1 | 96.3 |
| Heavy | 0 | 0 | 0 | 0 | 4 | 8 | 0 | 12 | 3 | 0 | 11 | 14 | 0 | 13 | 9 | 22 | 48 |
| % Heavy | 0 | 0 | 0 | 0 | 5.6 | 3.8 | 0 | 4.3 | 4.4 | 0 | 5.6 | 5.3 | 0 | 2.8 | 3.1 | 2.9 | 3.7 |



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File Name : 4855ac Site Code : 00004855 Start Date : 6/27/2023 Page No : 1

| | | | Grou | ups Printed- | Passenger | · + - Heavy | | | | |
|---------------|-------|--------------|------------|--------------|---------------|-------------|-------|-------------|------------|------------|
| | С | Id Pacific H | wy | C | DId Pacific F | łwy | Beln | nont Loop (| North) | |
| | | Southbound | b | | Northboun | d | | Eastbound | k k | |
| Start Time | Right | Thru | App. Total | Thru | Left | App. Total | Right | Left | App. Total | Int. Total |
| 04:00 PM | 24 | 97 | 121 | 52 | 4 | 56 | 11 | 17 | 28 | 205 |
| 04:15 PM | 10 | 92 | 102 | 63 | 4 | 67 | 7 | 25 | 32 | 201 |
| 04:30 PM | 27 | 103 | 130 | 54 | 8 | 62 | 4 | 25 | 29 | 221 |
| 04:45 PM | 18 | 123 | 141 | 47 | 3 | 50 | 8 | 24 | 32 | 223 |
| Total | 79 | 415 | 494 | 216 | 19 | 235 | 30 | 91 | 121 | 850 |
| | | | | | | | | | | |
| 05:00 PM | 30 | 94 | 124 | 39 | 7 | 46 | 11 | 23 | 34 | 204 |
| 05:15 PM | 18 | 129 | 147 | 34 | 5 | 39 | 11 | 26 | 37 | 223 |
| 05:30 PM | 20 | 85 | 105 | 39 | 4 | 43 | 8 | 31 | 39 | 187 |
| 05:45 PM | 16 | 76 | 92 | 45 | 7 | 52 | 7 | 19 | 26 | 170 |
| Total | 84 | 384 | 468 | 157 | 23 | 180 | 37 | 99 | 136 | 784 |
| | | | | | | | | | | |
| Grand Total | 163 | 799 | 962 | 373 | 42 | 415 | 67 | 190 | 257 | 1634 |
| Apprch % | 16.9 | 83.1 | | 89.9 | 10.1 | | 26.1 | 73.9 | | |
| Total % | 10 | 48.9 | 58.9 | 22.8 | 2.6 | 25.4 | 4.1 | 11.6 | 15.7 | |
| Passenger + | 161 | 776 | 937 | 353 | 39 | 392 | 66 | 184 | 250 | 1579 |
| % Passenger + | 98.8 | 97.1 | 97.4 | 94.6 | 92.9 | 94.5 | 98.5 | 96.8 | 97.3 | 96.6 |
| Heavy | 2 | 23 | 25 | 20 | 3 | 23 | 1 | 6 | 7 | 55 |
| % Heavy | 1.2 | 2.9 | 2.6 | 5.4 | 7.1 | 5.5 | 1.5 | 3.2 | 2.7 | 3.4 |

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File Name : 4855ac Site Code : 00004855 Start Date : 6/27/2023 Page No : 2

| | Ole | d Pacific H | wy | C | Id Pacific H | lwy | Beln | nont Loop (I | North) | |
|-------------------------|---------------|--------------|--------------|------|--------------|------------|-------|--------------|------------|------------|
| | 5 | Southbound | b | | Northboun | d | | Eastbound | k k | |
| Start Time | Right | Thru | App. Total | Thru | Left | App. Total | Right | Left | App. Total | Int. Total |
| Peak Hour Analysis Fre | om 04:00 PM | to 05:45 P | M - Peak 1 o | f 1 | | | | | | |
| Peak Hour for Entire In | tersection Be | egins at 04: | 30 PM | | | | | | | |
| 04:30 PM | 27 | 103 | 130 | 54 | 8 | 62 | 4 | 25 | 29 | 221 |
| 04:45 PM | 18 | 123 | 141 | 47 | 3 | 50 | 8 | 24 | 32 | 223 |
| 05:00 PM | 30 | 94 | 124 | 39 | 7 | 46 | 11 | 23 | 34 | 204 |
| 05:15 PM | 18 | 129 | 147 | 34 | 5 | 39 | 11 | 26 | 37 | 223 |
| Total Volume | 93 | 449 | 542 | 174 | 23 | 197 | 34 | 98 | 132 | 871 |
| % App. Total | 17.2 | 82.8 | | 88.3 | 11.7 | | 25.8 | 74.2 | | |
| PHF | .775 | .870 | .922 | .806 | .719 | .794 | .773 | .942 | .892 | .976 |
| Passenger + | 92 | 437 | 529 | 165 | 21 | 186 | 33 | 95 | 128 | 843 |
| % Passenger + | 98.9 | 97.3 | 97.6 | 94.8 | 91.3 | 94.4 | 97.1 | 96.9 | 97.0 | 96.8 |
| Heavy | 1 | 12 | 13 | 9 | 2 | 11 | 1 | 3 | 4 | 28 |
| % Heavy | 1.1 | 2.7 | 2.4 | 5.2 | 8.7 | 5.6 | 2.9 | 3.1 | 3.0 | 3.2 |



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| | | | Grou | ups Printed- | Passenger | · + - Heavy | | | | |
|---------------|-------|--------------|------------|--------------|---------------|-------------|-------|--------------|------------|------------|
| | C | Id Pacific H | wy | C | DId Pacific H | lwy | Beln | nont Loop (S | South) | |
| | | Southboun | d | | Northboun | d | | Eastbound | t k | |
| Start Time | Right | Thru | App. Total | Thru | Left | App. Total | Right | Left | App. Total | Int. Total |
| 04:00 PM | 8 | 99 | 107 | 57 | 5 | 62 | 7 | 3 | 10 | 179 |
| 04:15 PM | 2 | 96 | 98 | 62 | 4 | 66 | 4 | 3 | 7 | 171 |
| 04:30 PM | 4 | 100 | 104 | 60 | 4 | 64 | 6 | 4 | 10 | 178 |
| 04:45 PM | 2 | 134 | 136 | 50 | 2 | 52 | 9 | 1 | 10 | 198 |
| Total | 16 | 429 | 445 | 229 | 15 | 244 | 26 | 11 | 37 | 726 |
| | | | | | | | | | | |
| 05:00 PM | 2 | 103 | 105 | 49 | 3 | 52 | 3 | 2 | 5 | 162 |
| 05:15 PM | 2 | 143 | 145 | 39 | 1 | 40 | 4 | 3 | 7 | 192 |
| 05:30 PM | 0 | 99 | 99 | 39 | 1 | 40 | 11 | 2 | 13 | 152 |
| 05:45 PM | 1 | 80 | 81 | 46 | 1 | 47 | 3 | 4 | 7 | 135 |
| Total | 5 | 425 | 430 | 173 | 6 | 179 | 21 | 11 | 32 | 641 |
| | | | | | | | | | | |
| Grand Total | 21 | 854 | 875 | 402 | 21 | 423 | 47 | 22 | 69 | 1367 |
| Apprch % | 2.4 | 97.6 | | 95 | 5 | | 68.1 | 31.9 | | |
| Total % | 1.5 | 62.5 | 64 | 29.4 | 1.5 | 30.9 | 3.4 | 1.6 | 5 | |
| Passenger + | 21 | 833 | 854 | 383 | 21 | 404 | 45 | 22 | 67 | 1325 |
| % Passenger + | 100 | 97.5 | 97.6 | 95.3 | 100 | 95.5 | 95.7 | 100 | 97.1 | 96.9 |
| Heavy | 0 | 21 | 21 | 19 | 0 | 19 | 2 | 0 | 2 | 42 |
| % Heavy | 0 | 2.5 | 2.4 | 4.7 | 0 | 4.5 | 4.3 | 0 | 2.9 | 3.1 |

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| | 0 | ld Pacific H | wy | C | Id Pacific H | łwy | Beln | nont Loop (| South) | |
|-------------------------|--------------|---------------|---------------|------|--------------|------------|-------|-------------|------------|------------|
| | | Southbound | d | | Northboun | d | | Eastbound | b | |
| Start Time | Right | Thru | App. Total | Thru | Left | App. Total | Right | Left | App. Total | Int. Total |
| Peak Hour Analysis Fre | om 04:00 PN | /I to 05:45 F | PM - Peak 1 o | f 1 | | | | | | |
| Peak Hour for Entire In | tersection B | egins at 04: | :30 PM | | | | | | | |
| 04:30 PM | 4 | 100 | 104 | 60 | 4 | 64 | 6 | 4 | 10 | 178 |
| 04:45 PM | 2 | 134 | 136 | 50 | 2 | 52 | 9 | 1 | 10 | 198 |
| 05:00 PM | 2 | 103 | 105 | 49 | 3 | 52 | 3 | 2 | 5 | 162 |
| 05:15 PM | 2 | 143 | 145 | 39 | 1 | 40 | 4 | 3 | 7 | 192 |
| Total Volume | 10 | 480 | 490 | 198 | 10 | 208 | 22 | 10 | 32 | 730 |
| % App. Total | 2 | 98 | | 95.2 | 4.8 | | 68.8 | 31.2 | | |
| PHF | .625 | .839 | .845 | .825 | .625 | .813 | .611 | .625 | .800 | .922 |
| Passenger + | 10 | 468 | 478 | 187 | 10 | 197 | 20 | 10 | 30 | 705 |
| % Passenger + | 100 | 97.5 | 97.6 | 94.4 | 100 | 94.7 | 90.9 | 100 | 93.8 | 96.6 |
| Heavy | 0 | 12 | 12 | 11 | 0 | 11 | 2 | 0 | 2 | 25 |
| % Heavy | 0 | 2.5 | 2.4 | 5.6 | 0 | 5.3 | 9.1 | 0 | 6.3 | 3.4 |



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File Name : 4855ae Site Code : 00004855 Start Date : 6/27/2023 Page No : 1

| | | | Grou | ups Printed- | Passenger | + - Heavy | | | | |
|---------------|------|--------------|------------|--------------|-----------|------------|-------|--------------|------------|------------|
| | 0 | Id Pacific H | wy | Gre | en Mounta | in Rd | C | Id Pacific F | lwy | |
| | | Southbound | d b | | Westboun | d | | Northboun | d | |
| Start Time | Thru | Left | App. Total | Right | Left | App. Total | Right | Thru | App. Total | Int. Total |
| 04:00 PM | 88 | 17 | 105 | 9 | 8 | 17 | 14 | 56 | 70 | 192 |
| 04:15 PM | 78 | 21 | 99 | 20 | 4 | 24 | 9 | 47 | 56 | 179 |
| 04:30 PM | 84 | 20 | 104 | 20 | 5 | 25 | 14 | 43 | 57 | 186 |
| 04:45 PM | 113 | 28 | 141 | 18 | 7 | 25 | 8 | 33 | 41 | 207 |
| Total | 363 | 86 | 449 | 67 | 24 | 91 | 45 | 179 | 224 | 764 |
| | | | | | | | - | | | |
| 05:00 PM | 79 | 26 | 105 | 15 | 5 | 20 | 16 | 35 | 51 | 176 |
| 05:15 PM | 109 | 36 | 145 | 14 | 9 | 23 | 11 | 27 | 38 | 206 |
| 05:30 PM | 87 | 23 | 110 | 16 | 8 | 24 | 10 | 24 | 34 | 168 |
| 05:45 PM | 65 | 21 | 86 | 12 | 12 | 24 | 11 | 34 | 45 | 155 |
| Total | 340 | 106 | 446 | 57 | 34 | 91 | 48 | 120 | 168 | 705 |
| | | | | | | | | | | |
| Grand Total | 703 | 192 | 895 | 124 | 58 | 182 | 93 | 299 | 392 | 1469 |
| Apprch % | 78.5 | 21.5 | | 68.1 | 31.9 | | 23.7 | 76.3 | | |
| Total % | 47.9 | 13.1 | 60.9 | 8.4 | 3.9 | 12.4 | 6.3 | 20.4 | 26.7 | |
| Passenger + | 681 | 185 | 866 | 116 | 57 | 173 | 90 | 286 | 376 | 1415 |
| % Passenger + | 96.9 | 96.4 | 96.8 | 93.5 | 98.3 | 95.1 | 96.8 | 95.7 | 95.9 | 96.3 |
| Heavy | 22 | 7 | 29 | 8 | 1 | 9 | 3 | 13 | 16 | 54 |
| % Heavy | 3.1 | 3.6 | 3.2 | 6.5 | 1.7 | 4.9 | 3.2 | 4.3 | 4.1 | 3.7 |

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| | 0 | ld Pacific H | wy | Gre | een Mounta | in Rd | C | Id Pacific F | lwy | |
|-------------------------|--------------|---------------|---------------|-------|------------|------------|-------|--------------|------------|------------|
| | | Southbound | d | | Westboun | d | | Northboun | d | |
| Start Time | Thru | Left | App. Total | Right | Left | App. Total | Right | Thru | App. Total | Int. Total |
| Peak Hour Analysis Fr | om 04:00 PN | /I to 05:45 F | PM - Peak 1 o | f 1 | | | | | | |
| Peak Hour for Entire In | tersection B | egins at 04: | :30 PM | | | | | | | |
| 04:30 PM | 84 | 20 | 104 | 20 | 5 | 25 | 14 | 43 | 57 | 186 |
| 04:45 PM | 113 | 28 | 141 | 18 | 7 | 25 | 8 | 33 | 41 | 207 |
| 05:00 PM | 79 | 26 | 105 | 15 | 5 | 20 | 16 | 35 | 51 | 176 |
| 05:15 PM | 109 | 36 | 145 | 14 | 9 | 23 | 11 | 27 | 38 | 206 |
| Total Volume | 385 | 110 | 495 | 67 | 26 | 93 | 49 | 138 | 187 | 775 |
| % App. Total | 77.8 | 22.2 | | 72 | 28 | | 26.2 | 73.8 | | |
| PHF | .852 | .764 | .853 | .838 | .722 | .930 | .766 | .802 | .820 | .936 |
| Passenger + | 372 | 106 | 478 | 61 | 25 | 86 | 49 | 132 | 181 | 745 |
| % Passenger + | 96.6 | 96.4 | 96.6 | 91.0 | 96.2 | 92.5 | 100 | 95.7 | 96.8 | 96.1 |
| Heavy | 13 | 4 | 17 | 6 | 1 | 7 | 0 | 6 | 6 | 30 |
| % Heavy | 3.4 | 3.6 | 3.4 | 9.0 | 3.8 | 7.5 | 0 | 4.3 | 3.2 | 3.9 |



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| | | | | | | Grou | ups Prir | ted- Pas | senger | + - Hea | vy | | | | | | |
|---------------|-------|--------|-----------|------------|------------|-----------|-----------|------------|------------|---------|--------|------------|-------|------------|---------|------------|------------|
| | | Old Pa | cific Hv | vy | | E Sc | ott Ave | | | Goe | rig St | | | E Sco | ott Ave | | |
| | | South | nbound | | | Northw | estbour | nd | | North | bound | | | East | bound | | |
| Start Time | Right | Thru | Bear Left | App. Total | Bear Right | Bear Left | Hard Left | App. Total | Hard Right | Thru | Left | App. Total | Right | Bear Right | Left | App. Total | Int. Total |
| 04:00 PM | 22 | 26 | 49 | 97 | 54 | 11 | 1 | 66 | 0 | 2 | 0 | 2 | 5 | 3 | 11 | 19 | 184 |
| 04:15 PM | 16 | 24 | 50 | 90 | 48 | 12 | 1 | 61 | 0 | 0 | 0 | 0 | 6 | 6 | 7 | 19 | 170 |
| 04:30 PM | 17 | 28 | 50 | 95 | 44 | 21 | 3 | 68 | 0 | 1 | 2 | 3 | 6 | 3 | 11 | 20 | 186 |
| 04:45 PM | 20 | 29 | 69 | 118 | 36 | 13 | 1 | 50 | 0 | 1 | 0 | 1 | 3 | 3 | 6 | 12 | 181 |
| Total | 75 | 107 | 218 | 400 | 182 | 57 | 6 | 245 | 0 | 4 | 2 | 6 | 20 | 15 | 35 | 70 | 721 |
| | | | | | | | | | | | | | | | | | |
| 05:00 PM | 12 | 17 | 55 | 84 | 42 | 17 | 0 | 59 | 0 | 0 | 0 | 0 | 2 | 6 | 8 | 16 | 159 |
| 05:15 PM | 11 | 36 | 69 | 116 | 23 | 13 | 1 | 37 | 0 | 0 | 2 | 2 | 3 | 5 | 12 | 20 | 175 |
| 05:30 PM | 11 | 29 | 58 | 98 | 28 | 17 | 1 | 46 | 0 | 0 | 0 | 0 | 5 | 4 | 6 | 15 | 159 |
| 05:45 PM | 16 | 23 | 38 | 77 | 36 | 10 | 4 | 50 | 0 | 1 | 0 | 1 | 6 | 1 | 8 | 15 | 143 |
| Total | 50 | 105 | 220 | 375 | 129 | 57 | 6 | 192 | 0 | 1 | 2 | 3 | 16 | 16 | 34 | 66 | 636 |
| | | | | | | | | | | | | | | | | | |
| Grand Total | 125 | 212 | 438 | 775 | 311 | 114 | 12 | 437 | 0 | 5 | 4 | 9 | 36 | 31 | 69 | 136 | 1357 |
| Apprch % | 16.1 | 27.4 | 56.5 | | 71.2 | 26.1 | 2.7 | | 0 | 55.6 | 44.4 | | 26.5 | 22.8 | 50.7 | | |
| Total % | 9.2 | 15.6 | 32.3 | 57.1 | 22.9 | 8.4 | 0.9 | 32.2 | 0 | 0.4 | 0.3 | 0.7 | 2.7 | 2.3 | 5.1 | 10 | |
| Passenger + | 116 | 209 | 432 | 757 | 304 | 111 | 12 | 427 | 0 | 4 | 4 | 8 | 35 | 28 | 63 | 126 | 1318 |
| % Passenger + | 92.8 | 98.6 | 98.6 | 97.7 | 97.7 | 97.4 | 100 | 97.7 | 0 | 80 | 100 | 88.9 | 97.2 | 90.3 | 91.3 | 92.6 | 97.1 |
| Heavy | 9 | 3 | 6 | 18 | 7 | 3 | 0 | 10 | 0 | 1 | 0 | 1 | 1 | 3 | 6 | 10 | 39 |
| % Heavy | 7.2 | 1.4 | 1.4 | 2.3 | 2.3 | 2.6 | 0 | 2.3 | 0 | 20 | 0 | 11.1 | 2.8 | 9.7 | 8.7 | 7.4 | 2.9 |

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File Name : 4855af Site Code : 00004855 Start Date : 6/27/2023 Page No : 2

| | | Old Pa | cific Hw | /y | | E Sc | ott Ave | | | Goe | rig St | | | E Sco | ott Ave | | |
|---------------|-----------|---------|-----------|------------|------------|-----------|-----------|------------|------------|-------|--------|------------|-------|------------|---------|------------|------------|
| | | South | nbound | - | | Northw | estbour | nd | | North | bound | | | East | bound | | |
| Start Time | Right | Thru | Bear Left | App. Total | Bear Right | Bear Left | Hard Left | App. Total | Hard Right | Thru | Left | App. Total | Right | Bear Right | Left | App. Total | Int. Total |
| Peak Hour Ana | alysis Fi | rom 04: | 00 PM | to 05:45 | PM - P | eak 1 o | f 1 | | | | | | | | | | |
| Peak Hour for | Entire I | ntersec | tion Be | gins at 04 | 4:00 PN | 1 | | | | | | | | | | | |
| 04:00 PM | 22 | 26 | 49 | 97 | 54 | 11 | 1 | 66 | 0 | 2 | 0 | 2 | 5 | 3 | 11 | 19 | 184 |
| 04:15 PM | 16 | 24 | 50 | 90 | 48 | 12 | 1 | 61 | 0 | 0 | 0 | 0 | 6 | 6 | 7 | 19 | 170 |
| 04:30 PM | 17 | 28 | 50 | 95 | 44 | 21 | 3 | 68 | 0 | 1 | 2 | 3 | 6 | 3 | 11 | 20 | 186 |
| 04:45 PM | 20 | 29 | 69 | 118 | 36 | 13 | 1 | 50 | 0 | 1 | 0 | 1 | 3 | 3 | 6 | 12 | 181 |
| Total Volume | 75 | 107 | 218 | 400 | 182 | 57 | 6 | 245 | 0 | 4 | 2 | 6 | 20 | 15 | 35 | 70 | 721 |
| % App. Total | 18.8 | 26.8 | 54.5 | | 74.3 | 23.3 | 2.4 | | 0 | 66.7 | 33.3 | | 28.6 | 21.4 | 50 | | |
| PHF | .852 | .922 | .790 | .847 | .843 | .679 | .500 | .901 | .000 | .500 | .250 | .500 | .833 | .625 | .795 | .875 | .969 |
| Passenger + | 69 | 106 | 214 | 389 | 176 | 56 | 6 | 238 | 0 | 3 | 2 | 5 | 20 | 12 | 34 | 66 | 698 |
| % Passenger + | 92.0 | 99.1 | 98.2 | 97.3 | 96.7 | 98.2 | 100 | 97.1 | 0 | 75.0 | 100 | 83.3 | 100 | 80.0 | 97.1 | 94.3 | 96.8 |
| Heavy | 6 | 1 | 4 | 11 | 6 | 1 | 0 | 7 | 0 | 1 | 0 | 1 | 0 | 3 | 1 | 4 | 23 |
| % Heavy | 8.0 | 0.9 | 1.8 | 2.8 | 3.3 | 1.8 | 0 | 2.9 | 0 | 25.0 | 0 | 16.7 | 0 | 20.0 | 2.9 | 5.7 | 3.2 |



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Roundabout

File Name : 4855ag Site Code : 00004855 Start Date : 6/27/2023 Page No : 1

| | | | Grou | ups Printed- | Passenger | + - Heavy | | | | |
|---------------|------|--------------|------------|--------------|-------------|------------|-------|------------|------------|------------|
| | L | ewis River l | Rd | L | ewis River. | Rd | | E Scott Av | е | |
| | | Westbound | b | | Northboun | d | | Eastbound | l k | |
| Start Time | Thru | Left | App. Total | Right | Left | App. Total | Right | Thru | App. Total | Int. Total |
| 04:00 PM | 55 | 82 | 137 | 141 | 26 | 167 | 1 | 54 | 55 | 359 |
| 04:15 PM | 44 | 75 | 119 | 143 | 20 | 163 | 5 | 51 | 56 | 338 |
| 04:30 PM | 50 | 80 | 130 | 155 | 15 | 170 | 3 | 50 | 53 | 353 |
| 04:45 PM | 35 | 93 | 128 | 122 | 14 | 136 | 8 | 61 | 69 | 333 |
| Total | 184 | 330 | 514 | 561 | 75 | 636 | 17 | 216 | 233 | 1383 |
| | | | | | | | | | | |
| 05:00 PM | 45 | 82 | 127 | 138 | 17 | 155 | 5 | 58 | 63 | 345 |
| 05:15 PM | 30 | 76 | 106 | 173 | 15 | 188 | 7 | 70 | 77 | 371 |
| 05:30 PM | 27 | 97 | 124 | 161 | 12 | 173 | 9 | 55 | 64 | 361 |
| 05:45 PM | 31 | 77 | 108 | 170 | 18 | 188 | 4 | 41 | 45 | 341 |
| Total | 133 | 332 | 465 | 642 | 62 | 704 | 25 | 224 | 249 | 1418 |
| | | | | | | | | | | |
| Grand Total | 317 | 662 | 979 | 1203 | 137 | 1340 | 42 | 440 | 482 | 2801 |
| Apprch % | 32.4 | 67.6 | | 89.8 | 10.2 | | 8.7 | 91.3 | | |
| Total % | 11.3 | 23.6 | 35 | 42.9 | 4.9 | 47.8 | 1.5 | 15.7 | 17.2 | |
| Passenger + | 310 | 650 | 960 | 1187 | 134 | 1321 | 41 | 434 | 475 | 2756 |
| % Passenger + | 97.8 | 98.2 | 98.1 | 98.7 | 97.8 | 98.6 | 97.6 | 98.6 | 98.5 | 98.4 |
| Heavy | 7 | 12 | 19 | 16 | 3 | 19 | 1 | 6 | 7 | 45 |
| % Heavy | 2.2 | 1.8 | 1.9 | 1.3 | 2.2 | 1.4 | 2.4 | 1.4 | 1.5 | 1.6 |

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| | Le | ewis River I | ٦d | L | ewis River | Rd | | E Scott Av | e | |
|-------------------------|---------------|--------------|--------------|-------|------------|------------|-------|------------|------------|------------|
| | | Westbound | ł | | Northboun | d | | Eastbound | k k | |
| Start Time | Thru | Left | App. Total | Right | Left | App. Total | Right | Thru | App. Total | Int. Total |
| Peak Hour Analysis Fr | om 04:00 PN | 1 to 05:45 F | M - Peak 1 o | f 1 | | | | | | |
| Peak Hour for Entire In | tersection Be | egins at 05: | 00 PM | | | | | | | |
| 05:00 PM | 45 | 82 | 127 | 138 | 17 | 155 | 5 | 58 | 63 | 345 |
| 05:15 PM | 30 | 76 | 106 | 173 | 15 | 188 | 7 | 70 | 77 | 371 |
| 05:30 PM | 27 | 97 | 124 | 161 | 12 | 173 | 9 | 55 | 64 | 361 |
| 05:45 PM | 31 | 77 | 108 | 170 | 18 | 188 | 4 | 41 | 45 | 341 |
| Total Volume | 133 | 332 | 465 | 642 | 62 | 704 | 25 | 224 | 249 | 1418 |
| % App. Total | 28.6 | 71.4 | | 91.2 | 8.8 | | 10 | 90 | | |
| PHF | .739 | .856 | .915 | .928 | .861 | .936 | .694 | .800 | .808 | .956 |
| Passenger + | 132 | 328 | 460 | 636 | 61 | 697 | 25 | 223 | 248 | 1405 |
| % Passenger + | 99.2 | 98.8 | 98.9 | 99.1 | 98.4 | 99.0 | 100 | 99.6 | 99.6 | 99.1 |
| Heavy | 1 | 4 | 5 | 6 | 1 | 7 | 0 | 1 | 1 | 13 |
| % Heavy | 0.8 | 1.2 | 1.1 | 0.9 | 1.6 | 1.0 | 0 | 0.4 | 0.4 | 0.9 |



Heath & Associates Transportation Engineering Project: Logan's Landing Jurisdiction: Woodland, WA

Trip Generation Summary: Scenario 1 - All Shopping Plaza

| | Average Weekday Daily | | | | | | | | | | | | | | | | |
|----------------|---|------|----------------|-------|-------|-------|---------|--------|--------------------|--------|----------|---------|---------|---------|--------|-------------|--------|
| Development | Land Like | 1110 | Variable | Value | Pata | Distr | ibution | | Total Trips | | Internal | Capture | Pass-by | / Trips | P | rimary Trip | IS |
| Development | Land Ose | LOC | Valiable | value | nate | In | Out | In | Out | Total | % | Total | % | Total | In | Out | Total |
| Full Build-Out | Multifamily Housing (Low-Rise) | #220 | Dwelling Units | 272 | 6.74 | 50% | 50% | 916.6 | 916.6 | 1833.3 | 12.0% | 220.0 | 0.0% | 0.0 | 806.6 | 806.6 | 1613.3 |
| | Shopping Plaza (40-150k) - No Supermarket | #821 | 1,000 sq. ft. | 40.64 | 67.52 | 50% | 50% | 1372.0 | 1372.0 | 2744.0 | 12.0% | 329.3 | 40.00% | 965.9 | 724.4 | 724.4 | 1448.8 |
| | | | | | | | Totals | 2288.6 | 2288.6 | 4577.3 | Totals | 549.3 | Totals | 965.9 | 1531.1 | 1531.1 | 3062.1 |

| | Weekday AM Peak Hour | | | | | | | | | | | | | | | | |
|----------------|---|------|----------------|-------|------|-------|---------|------|--------------------|-------|----------|---------|---------|---------|------|-------------|-------|
| Development | Land Line | 1110 | Variable | Value | Data | Distr | ibution | | Total Trips | | Internal | Capture | Pass-by | / Trips | Р | rimary Trip | s |
| Development | Land Ose | LUC | variable | value | Rate | In | Out | In | Out | Total | % | Total | % | Total | In | Out | Total |
| Full Build Out | Multifamily Housing (Low-Rise) | #220 | Dwelling Units | 272 | 0.4 | 24% | 76% | 26.1 | 82.7 | 108.8 | 2.1% | 2.3 | 0.0% | 0.0 | 25.6 | 81.0 | 106.5 |
| Full Build-Out | Shopping Plaza (40-150k) - No Supermarket | #821 | 1,000 sq. ft. | 40.64 | 1.73 | 62% | 38% | 43.6 | 26.7 | 70.3 | 2.1% | 1.5 | 40% | 27.5 | 25.6 | 15.7 | 41.3 |
| | | | | | | | Totals | 69.7 | 109.4 | 179.1 | Totals | 3.8 | Totals | 27.5 | 51.2 | 96.6 | 147.8 |

| | Weekday PM Peak Hour | | | | | | | | | | | | | | | | |
|----------------|---|------|----------------|-------|------|-------|---------|-------|--------------------|-------|----------|---------|---------|---------|-------|-------------|-------|
| Dovelonment | Land Lico | 1110 | Variable | Value | Pata | Distr | ibution | | Total Trips | | Internal | Capture | Pass-by | / Trips | Р | rimary Trip | IS |
| Development | Land Ose | LOC | Valiable | value | nate | In | Out | In | Out | Total | % | Total | % | Total | In | Out | Total |
| Full Build-Out | Multifamily Housing (Low-Rise) | #220 | Dwelling Units | 272 | 0.51 | 63% | 37% | 87.4 | 51.3 | 138.7 | 21.9% | 30.4 | 0.0% | 0.0 | 68.3 | 40.1 | 108.3 |
| | Shopping Plaza (40-150k) - No Supermarket | #821 | 1,000 sq. ft. | 40.64 | 5.19 | 49% | 51% | 103.4 | 107.6 | 210.9 | 21.9% | 46.2 | 40.0% | 65.9 | 48.4 | 50.4 | 98.8 |
| | | | | | | | | 190.7 | 158.9 | 349.6 | Totals | 76.6 | Totals | 65.9 | 116.7 | 90.5 | 207.2 |

Sources:

Institute of Transportation Engineers, Trip Generation Manual, 11th Edition, (2021).

Pass-by rates were derived from the Institute of Transportation Engineers, 2021 Pass-By Tables for ITE Trip Gen Appendices (2021)

NCHRP 8-51 Internal Trip Capture Estimation Too

Heath & Associates Transportation Engineering Project: Logan's Landing Jurisdiction: Woodland, WA

Trip Generation Summary: Scenario 2 - Half Office, Half Strip Retail

| | Average Weekday Daily | | | | | | | | | | | | | | | | |
|----------------|--------------------------------|------|----------------|-------|-------|------|---------|--------|-------------|--------|----------|---------|---------|---------|--------|-------------|--------|
| Development | Land Lico | | Variable | Value | Pata | Dist | ibution | | Total Trips | | Internal | Capture | Pass-by | y Trips | Р | rimary Trip | IS |
| Development | Land Ose | LUC | Vallable | value | nate | In | Out | In | Out | Total | % | Total | % | Total | In | Out | Total |
| | Multifamily Housing (Low-Rise) | #220 | Dwelling Units | 272 | 6.74 | 50% | 50% | 916.6 | 916.6 | 1833.3 | 13.3% | 243.8 | 0.0% | 0.0 | 794.7 | 794.7 | 1589.5 |
| Full Build-Out | General Office | #710 | 1,000 sq. ft. | 20.32 | 10.84 | 50% | 50% | 110.1 | 110.1 | 220.3 | 13.3% | 29.3 | 0.0% | 0.0 | 95.5 | 95.5 | 191.0 |
| | Strip Retail Plaza (<40k) | #822 | 1,000 sq. ft. | 20.32 | 54.45 | 50% | 50% | 553.2 | 553.2 | 1106.4 | 13.3% | 147.2 | 40.00% | 383.7 | 287.8 | 287.8 | 575.6 |
| | | | | | | | Totals | 1580.0 | 1580.0 | 3160.0 | Totals | 420.3 | Totals | 383.7 | 1178.0 | 1178.0 | 2356.0 |

| | Weekday AM Peak Hour | | | | | | | | | | | | | | | | |
|----------------|--------------------------------|------|----------------|-------|------|-------|---------|------|-------------|-------|----------|---------|---------|---------|------|--------------|-------|
| Development | Land Line | | Variable | Value | Data | Distr | ibution | | Total Trips | | Internal | Capture | Pass-by | / Trips | P | Primary Trip | IS |
| Development | Land Ose | LUC | Variable | value | Rate | In | Out | In | Out | Total | % | Total | % | Total | In | Out | Total |
| | Multifamily Housing (Low-Rise) | #220 | Dwelling Units | 272 | 0.4 | 24% | 76% | 26.1 | 82.7 | 108.8 | 5.1% | 5.5 | 0.0% | 0.0 | 24.8 | 78.5 | 103.3 |
| Full Build-Out | General Office | #710 | 1,000 sq. ft. | 20.32 | 1.52 | 88% | 12% | 27.2 | 3.7 | 30.9 | 5.1% | 1.6 | 0.0% | 0.0 | 25.8 | 3.5 | 29.3 |
| | Strip Retail Plaza (<40k) | #822 | 1,000 sq. ft. | 20.32 | 2.36 | 60% | 40% | 28.8 | 19.2 | 48.0 | 5.1% | 2.4 | 40% | 18.2 | 16.4 | 10.9 | 27.3 |
| | | | | | | | Totals | 82.1 | 105.6 | 187.6 | Totals | 9.6 | Totals | 18.2 | 67.0 | 92.9 | 159.9 |

| | Weekday PM Peak Hour | | | | | | | | | | | | | | | | |
|----------------|--------------------------------|------|----------------|-------|------|-------|---------|-------|--------------------|-------|----------|---------|---------|---------|-------|-------------|-------|
| Development | Land Line | | Variable | Malua | Bete | Distr | ibution | | Total Trips | | Internal | Capture | Pass-by | y Trips | P | rimary Trip |)S |
| Development | Land Ose | LUC | variable | value | Rate | In | Out | In | Out | Total | % | Total | % | Total | In | Out | Total |
| | Multifamily Housing (Low-Rise) | #220 | Dwelling Units | 272 | 0.51 | 63% | 37% | 87.4 | 51.3 | 138.7 | 21.5% | 29.8 | 0.0% | 0.0 | 68.6 | 40.3 | 108.9 |
| Full Build-Out | General Office | #710 | 1,000 sq. ft. | 20.32 | 1.44 | 17% | 83% | 5.0 | 24.3 | 29.3 | 21.5% | 6.3 | 0.0% | 0.0 | 3.9 | 19.1 | 23.0 |
| | Strip Retail Plaza (<40k) | #822 | 1,000 sq. ft. | 20.32 | 6.59 | 50% | 50% | 67.0 | 67.0 | 133.9 | 21.5% | 28.8 | 40.0% | 42.0 | 31.5 | 31.5 | 63.1 |
| | | | | | | | | 159.3 | 142.6 | 301.9 | Totals | 64.9 | Totals | 42.0 | 104.0 | 90.9 | 194.9 |

Sources:

Institute of Transportation Engineers, Trip Generation Manual, 11th Edition, (2021).

Pass-by rates were derived from the Institute of Transportation Engineers, 2021 Pass-By Tables for ITE Trip Gen Appendices (2021)

NCHRP 8-51 Internal Trip Capture Estimation Too

| | NCHRP 8-51 Internal Trip C | Cap | oture Estimation Tool | |
|-----------------------|----------------------------|-----|-----------------------|--------------------|
| Project Name: | Logan's Landing | | Organization: | Heath & Associates |
| Project Location: | Woodland, WA | | Performed By: | PW |
| Scenario Description: | Full Buildout | | Date: | 7/15/2023 |
| Analysis Year: | 2025 | | Checked By: | |
| Analysis Period: | AM Street Peak Hour | | Date: | |

| | Table 1 | -A: Base Vehicl | e-Trip Generatior | ı Es | timates (Single-Use Si | te Estimate) | |
|----------------------------------|-----------------------|----------------------------|-------------------|------|------------------------|-------------------------|---------|
| Land Lies | Developme | ent Data (<i>For In</i> i | formation Only) | | | Estimated Vehicle-Trips | |
| Land Use | ITE LUCs ¹ | Quantity | Units | | Total | Entering | Exiting |
| Office | 710 | 20,320 | sq. ft. | | 30.9 | 27.2 | 3.7 |
| Retail | 822 | 20,320 | sq. ft. | | 48 | 28.8 | 19.2 |
| Restaurant | | | | | 0 | | |
| Cinema/Entertainment | | | | | 0 | | |
| Residential | 220 | 272 | Dwelling Units | | 108.8 | 26.1 | 82.7 |
| Hotel | | | | | 0 | | |
| All Other Land Uses ² | | | | | 0 | | |
| Total | | | | | 187.7 | 82.1 | 105.6 |

| | | Table 2-A: | Mode Split and Veh | icle | Occupancy Estimate | 6 | |
|----------------------------------|-----------|-------------|--------------------|------|--------------------|---------------|-----------------|
| Land Line | | Entering Tr | ps | | | Exiting Trips | |
| Land Ose | Veh. Occ. | % Transit | % Non-Motorized | | Veh. Occ. | % Transit | % Non-Motorized |
| Office | | | | | | | |
| Retail | | | | | | | |
| Restaurant | | | | | | | |
| Cinema/Entertainment | | | | | | | |
| Residential | | | | | | | |
| Hotel | | | | | | | |
| All Other Land Uses ² | | | | | | | |

| | Table | 3-A: Average La | and Use Interchan | ge Distances (Feet Walking | g Distance) | |
|----------------------|--------|-----------------|-------------------|----------------------------|-------------|-------|
| Origin (From) | | | | Destination (To) | | |
| Ongin (From) | Office | Retail | Restaurant | Cinema/Entertainment | Residential | Hotel |
| Office | | | | | | |
| Retail | | | | | | |
| Restaurant | | | | | | |
| Cinema/Entertainment | | | | | | |
| Residential | | | | | | |
| Hotel | | | | | | |

| | | Table 4-A: In | nternal Person-Trip | p Origin-Destination Matrix | * | |
|----------------------|--------|---------------|---------------------|-----------------------------|-------------|-------|
| Origin (From) | | | | Destination (To) | | |
| | Office | Retail | Restaurant | Cinema/Entertainment | Residential | Hotel |
| Office | | 1 | 0 | 0 | 0 | 0 |
| Retail | 1 | | 0 | 0 | 1 | 0 |
| Restaurant | 0 | 0 | | 0 | 0 | 0 |
| Cinema/Entertainment | 0 | 0 | 0 | | 0 | 0 |
| Residential | 1 | 1 | 0 | 0 | | 0 |
| Hotel | 0 | 0 | 0 | 0 | 0 | |

| Table 5-A | : Computatio | ons Summary | | Table 6-A: Internal | Trip Capture Percenta | ges by Land Use |
|---|--------------|-------------|---------|----------------------|-----------------------|-----------------|
| | Total | Entering | Exiting | Land Use | Entering Trips | Exiting Trips |
| All Person-Trips | 188 | 82 | 106 | Office | 7% | 25% |
| Internal Capture Percentage | 5% | 6% | 5% | Retail | 7% | 11% |
| | | | | Restaurant | N/A | N/A |
| External Vehicle-Trips ³ | 178 | 77 | 101 | Cinema/Entertainment | N/A | N/A |
| External Transit-Trips ⁴ | 0 | 0 | 0 | Residential | 4% | 2% |
| External Non-Motorized Trips ⁴ | 0 | 0 | 0 | Hotel | N/A | N/A |

| Land Use Codes (LUCs) from Trip Generation informational Report, published by the institute of Transportation Engineers. |
|---|
| ² Total estimate for all other land uses at mixed-use development site-not subject to internal trip capture computations in this estimator |
| ³ Vehicle-trips computed using the mode split and vehicle occupancy values provided in Table 2-A |

⁴Person-Trips

*Indicates computation that has been rounded to the nearest whole number.

Estimation Tool Developed by the Texas Transportation Institute

| Project Name: | Logan's Landing |
|------------------|---------------------|
| Analysis Period: | AM Street Peak Hour |

| Table 7-A: Conversion of Vehicle-Trip Ends to Person-Trip Ends | | | | | | | | | | |
|--|-----------|-------------------|---------------|---|------------------------------|---------------|---------------|--|--|--|
| | Tab | le 7-A (D): Enter | ing Trips | | Table 7-A (O): Exiting Trips | | | | | |
| Land Ose | Veh. Occ. | Vehicle-Trips | Person-Trips* | 1 | Veh. Occ. | Vehicle-Trips | Person-Trips* | | | |
| Office | 1.00 | 27.2 | 27 | 1 | 1.00 | 3.7 | 4 | | | |
| Retail | 1.00 | 28.8 | 29 | 1 | 1.00 | 19.2 | 19 | | | |
| Restaurant | 1.00 | 0 | 0 | 1 | 1.00 | 0 | 0 | | | |
| Cinema/Entertainment | 1.00 | 0 | 0 | 1 | 1.00 | 0 | 0 | | | |
| Residential | 1.00 | 26.1 | 26 | 1 | 1.00 | 82.7 | 83 | | | |
| Hotel | 1.00 | 0 | 0 |] | 1.00 | 0 | 0 | | | |

| Table 8-A (O): Internal Person-Trip Origin-Destination Matrix (Computed at Origin) | | | | | | | | | | |
|--|------------------|--------|------------|----------------------|-------------|-------|--|--|--|--|
| Origin (From) | Destination (To) | | | | | | | | | |
| Origin (From) | Office | Retail | Restaurant | Cinema/Entertainment | Residential | Hotel | | | | |
| Office | | 1 | 3 | 0 | 0 | 0 | | | | |
| Retail | 6 | | 2 | 0 | 3 | 0 | | | | |
| Restaurant | 0 | 0 | | 0 | 0 | 0 | | | | |
| Cinema/Entertainment | 0 | 0 | 0 | | 0 | 0 | | | | |
| Residential | 2 | 1 | 17 | 0 | | 0 | | | | |
| Hotel | 0 | 0 | 0 | 0 | 0 | | | | | |

| Table 8-A (D): Internal Person-Trip Origin-Destination Matrix (Computed at Destination) | | | | | | | | | | |
|---|------------------|--------|------------|----------------------|-------------|-------|--|--|--|--|
| | Destination (To) | | | | | | | | | |
| Origin (From) | Office | Retail | Restaurant | Cinema/Entertainment | Residential | Hotel | | | | |
| Office | | 9 | 0 | 0 | 0 | 0 | | | | |
| Retail | 1 | | 0 | 0 | 1 | 0 | | | | |
| Restaurant | 4 | 2 | | 0 | 1 | 0 | | | | |
| Cinema/Entertainment | 0 | 0 | 0 | | 0 | 0 | | | | |
| Residential | 1 | 5 | 0 | 0 | | 0 | | | | |
| Hotel | 1 | 1 | 0 | 0 | 0 | | | | | |

| Table 9-A (D): Internal and External Trips Summary (Entering Trips) | | | | | | | | | | |
|---|----------|------------------|-------|--|-------------------------|----------------------|----------------------------|--|--|--|
| Destination Land Has | | Person-Trip Esti | mates | | External Trips by Mode* | | | | | |
| Destination Land Use | Internal | External | Total | | Vehicles ¹ | Transit ² | Non-Motorized ² | | | |
| Office | 2 | 25 | 27 | | 25 | 0 | 0 | | | |
| Retail | 2 | 27 | 29 | | 27 | 0 | 0 | | | |
| Restaurant | 0 | 0 | 0 | | 0 | 0 | 0 | | | |
| Cinema/Entertainment | 0 | 0 | 0 | | 0 | 0 | 0 | | | |
| Residential | 1 | 25 | 26 | | 25 | 0 | 0 | | | |
| Hotel | 0 | 0 | 0 | | 0 | 0 | 0 | | | |
| All Other Land Uses ³ | 0 | 0 | 0 | | 0 | 0 | 0 | | | |

| Table 9-A (O): Internal and External Trips Summary (Exiting Trips) | | | | | | | | | |
|--|----------|-------------------|-------|--|-------------------------|----------------------|----------------------------|--|--|
| Original and the | | Person-Trip Estii | mates | | External Trips by Mode* | | | | |
| Oligin Land Ose | Internal | External | Total | | Vehicles ¹ | Transit ² | Non-Motorized ² | | |
| Office | 1 | 3 | 4 | | 3 | 0 | 0 | | |
| Retail | 2 | 17 | 19 | | 17 | 0 | 0 | | |
| Restaurant | 0 | 0 | 0 | | 0 | 0 | 0 | | |
| Cinema/Entertainment | 0 | 0 | 0 | | 0 | 0 | 0 | | |
| Residential | 2 | 81 | 83 | | 81 | 0 | 0 | | |
| Hotel | 0 | 0 | 0 | | 0 | 0 | 0 | | |
| All Other Land Uses ³ | 0 | 0 | 0 | | 0 | 0 | 0 | | |

¹Vehicle-trips computed using the mode split and vehicle occupancy values provided in Table 2-A

²Person-Trips

³Total estimate for all other land uses at mixed-use development site-not subject to internal trip capture computations in this estimator

*Indicates computation that has been rounded to the nearest whole number.

| NCHRP 8-51 Internal Trip Capture Estimation Tool | | | | | | | | | | |
|--|---------------------|---------------|--------------------|-----------|--|--|--|--|--|--|
| Project Name: | Logan's Landing | Organization: | Heath & Associates | | | | | | | |
| Project Location: | Woodland, WA | | Performed By: | PW | | | | | | |
| Scenario Description: | Full Buildout | | Date: | 7/15/2023 | | | | | | |
| Analysis Year: | 2025 | | Checked By: | | | | | | | |
| Analysis Period: | PM Street Peak Hour | | Date: | | | | | | | |

| Table 1-P: Base Vehicle-Trip Generation Estimates (Single-Use Site Estimate) | | | | | | | | |
|--|-----------------------|----------------------------|-----------------|--|-------------------------|----------|---------|--|
| Land Llas | Developme | ent Data (<i>For In</i> i | formation Only) | | Estimated Vehicle-Trips | | | |
| Land Use | ITE LUCs ¹ | Quantity | Units | | Total | Entering | Exiting | |
| Office | 710 | 20,320 | sq. ft. | | 29.3 | 5 | 24.3 | |
| Retail | 822 | 20,320 | sq. ft. | | 134 | 67 | 67 | |
| Restaurant | | | | | 0 | | | |
| Cinema/Entertainment | | | | | 0 | | | |
| Residential | 220 | 272 | Dwelling Units | | 138.7 | 87.4 | 51.3 | |
| Hotel | | | | | 0 | | | |
| All Other Land Uses ² | | | | | 0 | | | |
| Total | | | | | 302 | 159.4 | 142.6 | |

| Table 2-P: Mode Split and Vehicle Occupancy Estimates | | | | | | | | | |
|---|----------------|-----------|-----------------|--|---------------|-----------|-----------------|--|--|
| | Entering Trips | | | | Exiting Trips | | | | |
| Land Use | Veh. Occ. | % Transit | % Non-Motorized | | Veh. Occ. | % Transit | % Non-Motorized | | |
| Office | | | | | | | | | |
| Retail | | | | | | | | | |
| Restaurant | | | | | | | | | |
| Cinema/Entertainment | | | | | | | | | |
| Residential | | | | | | | | | |
| Hotel | | | | | | | | | |
| All Other Land Uses ² | | | | | | | | | |

| Table 3-P: Average Land Use Interchange Distances (Feet Walking Distance) | | | | | | | | | |
|---|--------|------------------|------------|----------------------|-------------|-------|--|--|--|
| | | Destination (To) | | | | | | | |
| Ongin (From) | Office | Retail | Restaurant | Cinema/Entertainment | Residential | Hotel | | | |
| Office | | | | | | | | | |
| Retail | | | | | | | | | |
| Restaurant | | | | | | | | | |
| Cinema/Entertainment | | | | | | | | | |
| Residential | | | | | | | | | |
| Hotel | | | | | | | | | |

| Table 4-P: Internal Person-Trip Origin-Destination Matrix* | | | | | | | | | | |
|--|------------------|--------|------------|----------------------|-------------|-------|--|--|--|--|
| Origin (From) | Destination (To) | | | | | | | | | |
| | Office | Retail | Restaurant | Cinema/Entertainment | Residential | Hotel | | | | |
| Office | | 5 | 0 | 0 | 0 | 0 | | | | |
| Retail | 1 | | 0 | 0 | 17 | 0 | | | | |
| Restaurant | 0 | 0 | | 0 | 0 | 0 | | | | |
| Cinema/Entertainment | 0 | 0 | 0 | | 0 | 0 | | | | |
| Residential | 2 | 7 | 0 | 0 | | 0 | | | | |
| Hotel | 0 | 0 | 0 | 0 | 0 | | | | | |

| Table 5-P | : Computatio | ons Summary | | Table 6-P: Internal | Trip Capture Percenta | ges by Land Use |
|---|--------------|-------------|---------|----------------------|------------------------------|-----------------|
| | Total | Entering | Exiting | Land Use | Entering Trips | Exiting Trips |
| All Person-Trips | 301 | 159 | 142 | Office | 60% | 21% |
| Internal Capture Percentage | 21% | 20% | 23% | Retail | 18% | 27% |
| | | | | Restaurant | N/A | N/A |
| External Vehicle-Trips ³ | 237 | 127 | 110 | Cinema/Entertainment | N/A | N/A |
| External Transit-Trips ⁴ | 0 | 0 | 0 | Residential | 20% | 18% |
| External Non-Motorized Trips ⁴ | 0 | 0 | 0 | Hotel | N/A | N/A |

| Land Use Codes (LUCs) from <i>Trip Generation Informational Report</i> , published by the Institute of Transportation Engineers. | |
|---|--|
| ² Total estimate for all other land uses at mixed-use development site-not subject to internal trip capture computations in this estimator | |

³Vehicle-trips computed using the mode split and vehicle occupancy values provided in Table 2-P ⁴Person-Trips *Indicates computation that has been rounded to the nearest whole number.

Estimation Tool Developed by the Texas Transportation Institute

| Project Name: | Logan's Landing |
|------------------|---------------------|
| Analysis Period: | PM Street Peak Hour |

| | Та | ble 7-P: Conver | sion of Vehicle-Tr | ip E | Ends to Person-Trip End | ls | |
|----------------------|-----------|-------------------|--------------------|------|-------------------------|-----------------------------|---------------|
| | Table | 7-P (D): Entering | g Trips | | Т | able 7-P (O): Exiting Trips | |
| Land Use | Veh. Occ. | Vehicle-Trips | Person-Trips* | Î | Veh. Occ. | Vehicle-Trips | Person-Trips* |
| Office | 1.00 | 5 | 5 | | 1.00 | 24.3 | 24 |
| Retail | 1.00 | 67 | 67 | | 1.00 | 67 | 67 |
| Restaurant | 1.00 | 0 | 0 | | 1.00 | 0 | 0 |
| Cinema/Entertainment | 1.00 | 0 | 0 | | 1.00 | 0 | 0 |
| Residential | 1.00 | 87.4 | 87 | | 1.00 | 51.3 | 51 |
| Hotel | 1.00 | 0 | 0 | | 1.00 | 0 | 0 |

| | Table 8-P (0 | D): Internal Pers | on-Trip Origin-De | stination Matrix (Computed | at Origin) | |
|----------------------|--------------|-------------------|-------------------|----------------------------|-------------|-------|
| Origin (From) | | | | Destination (To) | | |
| Oligin (From) | Office | Retail | Restaurant | Cinema/Entertainment | Residential | Hotel |
| Office | | 5 | 1 | 0 | 0 | 0 |
| Retail | 1 | | 19 | 3 | 17 | 3 |
| Restaurant | 0 | 0 | | 0 | 0 | 0 |
| Cinema/Entertainment | 0 | 0 | 0 | | 0 | 0 |
| Residential | 2 | 21 | 11 | 0 | | 2 |
| Hotel | 0 | 0 | 0 | 0 | 0 | |

| | Table 8-P (D): | Internal Person | -Trip Origin-Desti | nation Matrix (Computed at | Destination) | |
|----------------------|----------------|-----------------|--------------------|----------------------------|--------------|-------|
| Origin (From) | | | | Destination (To) | | |
| Oligin (Floin) | Office | Retail | Restaurant | Cinema/Entertainment | Residential | Hotel |
| Office | | 5 | 0 | 0 | 3 | 0 |
| Retail | 2 | | 0 | 0 | 40 | 0 |
| Restaurant | 2 | 34 | | 0 | 14 | 0 |
| Cinema/Entertainment | 0 | 3 | 0 | | 3 | 0 |
| Residential | 3 | 7 | 0 | 0 | | 0 |
| Hotel | 0 | 1 | 0 | 0 | 0 | |

| | Tal | ole 9-P (D): Inter | nal and External T | rips | Summary (Entering Tr | ips) | |
|----------------------------------|----------|--------------------|--------------------|------|-----------------------|-------------------------|----------------------------|
| Destination Land Llas | P | erson-Trip Estima | ates | | | External Trips by Mode* | |
| Destination Land Ose | Internal | External | Total | 1 | Vehicles ¹ | Transit ² | Non-Motorized ² |
| Office | 3 | 2 | 5 | | 2 | 0 | 0 |
| Retail | 12 | 55 | 67 | | 55 | 0 | 0 |
| Restaurant | 0 | 0 | 0 | | 0 | 0 | 0 |
| Cinema/Entertainment | 0 | 0 | 0 | | 0 | 0 | 0 |
| Residential | 17 | 70 | 87 | | 70 | 0 | 0 |
| Hotel | 0 | 0 | 0 | | 0 | 0 | 0 |
| All Other Land Uses ³ | 0 | 0 | 0 | | 0 | 0 | 0 |

| | Та | ble 9-P (O): Inter | nal and External | Trip | s Summary (Exiting Tri | ps) | |
|----------------------------------|----------|--------------------|------------------|------|------------------------|-------------------------|----------------------------|
| | P | erson-Trip Estima | ites | | | External Trips by Mode* | |
| Origin Land Use | Internal | External | Total | 1 | Vehicles ¹ | Transit ² | Non-Motorized ² |
| Office | 5 | 19 | 24 | | 19 | 0 | 0 |
| Retail | 18 | 49 | 67 | | 49 | 0 | 0 |
| Restaurant | 0 | 0 | 0 | | 0 | 0 | 0 |
| Cinema/Entertainment | 0 | 0 | 0 | | 0 | 0 | 0 |
| Residential | 9 | 42 | 51 | | 42 | 0 | 0 |
| Hotel | 0 | 0 | 0 | | 0 | 0 | 0 |
| All Other Land Uses ³ | 0 | 0 | 0 | | 0 | 0 | 0 |

¹Vehicle-trips computed using the mode split and vehicle occupancy values provided in Table 2-P

²Person-Trips

³Total estimate for all other land uses at mixed-use development site-not subject to internal trip capture computations in this estimator *Indicates computation that has been rounded to the nearest whole number.

₩ Site: 1 [1. I-5 SB Ramps & Dike Access Road (Site Folder: General)]

Output produced by SIDRA INTERSECTION Version: 9.1.3.210

Existing 2023 PM Peak Hour Site Category: (None) Roundabout

| Vehic | cle Mo | ovement | Perfor | man | се | | | | | | | | | | |
|-----------|----------|--------------|------------------------------|---------------------------|------------------------------|----------------------------|---------------------|-----------------------|---------------------|----------------------------|---------------------------------|--------------|----------------------|---------------------------|-----------------------|
| Mov ID | Turn | Mov Class | Dem F [Total veh/h | nand lows HV] % | Ar Fl [Total veh/h | rival lows HV] % | Deg. Satn v/c | Aver. Delay sec | Level of Service | 95% Qı [Veh. veh | Back Of Jeue Dist] ft | Prop. Que | Eff. Stop Rate | Aver. No. of Cycles | Aver. Speed mph |
| East: | Dike A | ccess Ro | ad | | | | | | | | | | | | |
| 1 | L2 | All MCs | 105 | 5.1 | 105 | 5.1 | 0.330 | 9.8 | LOS A | 0.0 | 0.0 | 0.00 | 0.47 | 0.00 | 35.1 |
| 6 | T1 | All MCs | 354 | 3.3 | 354 | 3.3 | 0.330 | 3.8 | LOS A | 0.0 | 0.0 | 0.00 | 0.47 | 0.00 | 36.0 |
| Appro | ach | | 460 | 3.7 | 460 | 3.7 | 0.330 | 5.2 | LOS A | 0.0 | 0.0 | 0.00 | 0.47 | 0.00 | 35.8 |
| North: | : I-5 SI | 3 Off-Ram | ıp | | | | | | | | | | | | |
| 7 | L2 | All MCs | 153 | 9.7 | 153 | 9.7 | 0.380 | 13.4 | LOS B | 2.3 | 60.3 | 0.64 | 0.67 | 0.64 | 32.7 |
| 4 | T1 | All MCs | 5 | 1.0 | 5 | 1.0 | 0.380 | 6.8 | LOS A | 2.3 | 60.3 | 0.64 | 0.67 | 0.64 | 33.6 |
| 14 | R2 | All MCs | 195 | 3.3 | 195 | 3.3 | 0.380 | 7.1 | LOS A | 2.3 | 60.3 | 0.64 | 0.67 | 0.64 | 33.3 |
| Appro | ach | | 353 | 6.0 | 353 | 6.0 | 0.380 | 9.8 | LOS A | 2.3 | 60.3 | 0.64 | 0.67 | 0.64 | 33.0 |
| West: | Dike / | Access Ro | bad | | | | | | | | | | | | |
| 2 | T1 | All MCs | 557 | 1.0 | 557 | 1.0 | 0.717 | 7.9 | LOS A | 8.7 | 221.1 | 0.80 | 0.68 | 0.91 | 34.2 |
| 12 | R2 | All MCs | 244 | 2.6 | 244 | 2.6 | 0.717 | 8.2 | LOS A | 8.7 | 221.1 | 0.80 | 0.68 | 0.91 | 33.9 |
| Appro | ach | | 801 | 1.5 | 801 | 1.5 | 0.717 | 8.0 | LOS A | 8.7 | 221.1 | 0.80 | 0.68 | 0.91 | 34.1 |
| All Ve | hicles | | 1614 | 3.1 | 1614 | 3.1 | 0.717 | 7.6 | LOS A | 8.7 | 221.1 | 0.54 | 0.62 | 0.59 | 34.3 |

Site Level of Service (LOS) Method: Delay & Degree of Saturation (SIDRA). Site LOS Method is specified in the Parameter Settings dialog (Options tab).

Roundabout LOS Method: Same as Signalised Intersections.

Vehicle movement LOS values are based on average delay and v/c ratio (degree of saturation) per movement.

Intersection and Approach LOS values are based on average delay for all movements (v/c not used).

Roundabout Capacity Model: SIDRA HCM.

Delay Model: SIDRA Standard (Control Delay: Geometric Delay is included).

Queue Model: SIDRA queue estimation methods are used for Back of Queue and Queue at Start of Gap.

Gap-Acceptance Capacity Formula: SIDRA Standard (Akçelik M3D).

HV (%) values are calculated for All Movement Classes of All Heavy Vehicle Model Designation.

Arrival Flows used in performance calculations are adjusted to include any Initial Queued Demand and Upstream Capacity Constraint effects.

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SITE LAYOUT V Site: 1 [1. I-5 SB Ramps & Dike Access Road (Site Folder: General)]

Existing 2023 PM Peak Hour Site Category: (None) Roundabout

Layout pictures are schematic functional drawings reflecting input data. They are not design drawings.



₩ Site: 2 [2. I-5 NB Ramp & Dike Access Road (Site Folder: General)]

Output produced by SIDRA INTERSECTION Version: 9.1.3.210

Exsiting 2023 PM Peak Hour Site Category: (None) Roundabout

| Vehic | le Mo | ovement | Perfor | man | ce | | | | | | | | | | |
|-----------|---------|--------------|-------------------------------|---------------------------|------------------------------|---------------------------|---------------------|-----------------------|---------------------|------------------------------|---------------------------------|--------------|----------------------|---------------------------|-----------------------|
| Mov ID | Turn | Mov Class | Derr F [Total veh/h | nand Iows HV] % | Ar Fl [Total veh/h | rival lows HV] % | Deg. Satn v/c | Aver. Delay sec | Level of Service | 95% [Qu [Veh. veh | Back Of ieue Dist] ft | Prop. Que | Eff. Stop Rate | Aver. No. of Cycles | Aver. Speed mph |
| South | : I-5 N | B Off-Ran | np | | | | | | | | | | | | |
| 3 | L2 | All MCs | 210 | 5.6 | 210 | 5.6 | 0.393 | 16.9 | LOS B | 2.5 | 66.3 | 0.80 | 0.79 | 0.84 | 30.5 |
| 8 | T1 | All MCs | 1 | 1.0 | 1 | 1.0 | 0.393 | 10.2 | LOS B | 2.5 | 66.3 | 0.80 | 0.79 | 0.84 | 31.2 |
| 18 | R2 | All MCs | 72 | 4.4 | 72 | 4.4 | 0.393 | 10.8 | LOS B | 2.5 | 66.3 | 0.80 | 0.79 | 0.84 | 30.9 |
| Appro | ach | | 283 | 5.3 | 283 | 5.3 | 0.393 | 15.3 | LOS B | 2.5 | 66.3 | 0.80 | 0.79 | 0.84 | 30.6 |
| East: | Dike A | ccess Ro | ad | | | | | | | | | | | | |
| 6 | T1 | All MCs | 221 | 3.8 | 221 | 3.8 | 0.341 | 7.3 | LOS A | 2.2 | 56.5 | 0.70 | 0.64 | 0.70 | 34.5 |
| 16 | R2 | All MCs | 76 | 5.6 | 76 | 5.6 | 0.341 | 7.6 | LOS A | 2.2 | 56.5 | 0.70 | 0.64 | 0.70 | 34.1 |
| Appro | ach | | 297 | 4.3 | 297 | 4.3 | 0.341 | 7.4 | LOS A | 2.2 | 56.5 | 0.70 | 0.64 | 0.70 | 34.4 |
| West: | Dike / | Access Ro | ad | | | | | | | | | | | | |
| 5 | L2 | All MCs | 310 | 3.1 | 310 | 3.1 | 0.569 | 9.7 | LOS A | 0.0 | 0.0 | 0.00 | 0.53 | 0.00 | 34.7 |
| 2 | T1 | All MCs | 487 | 2.8 | 487 | 2.8 | 0.569 | 3.7 | LOS A | 0.0 | 0.0 | 0.00 | 0.53 | 0.00 | 35.6 |
| Appro | ach | | 797 | 2.9 | 797 | 2.9 | 0.569 | 6.1 | LOS A | 0.0 | 0.0 | 0.00 | 0.53 | 0.00 | 35.2 |
| All Ve | hicles | | 1377 | 3.7 | 1377 | 3.7 | 0.569 | 8.2 | LOS A | 2.5 | 66.3 | 0.32 | 0.60 | 0.32 | 34.0 |

Site Level of Service (LOS) Method: Delay & Degree of Saturation (SIDRA). Site LOS Method is specified in the Parameter Settings dialog (Options tab).

Roundabout LOS Method: Same as Signalised Intersections.

Vehicle movement LOS values are based on average delay and v/c ratio (degree of saturation) per movement.

Intersection and Approach LOS values are based on average delay for all movements (v/c not used).

Roundabout Capacity Model: SIDRA HCM.

Delay Model: SIDRA Standard (Control Delay: Geometric Delay is included).

Queue Model: SIDRA queue estimation methods are used for Back of Queue and Queue at Start of Gap.

Gap-Acceptance Capacity Formula: SIDRA Standard (Akçelik M3D).

HV (%) values are calculated for All Movement Classes of All Heavy Vehicle Model Designation.

Arrival Flows used in performance calculations are adjusted to include any Initial Queued Demand and Upstream Capacity Constraint effects.

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SITE LAYOUT V Site: 2 [2. I-5 NB Ramp & Dike Access Road (Site Folder: General)]

Exsiting 2023 PM Peak Hour Site Category: (None) Roundabout

Layout pictures are schematic functional drawings reflecting input data. They are not design drawings.



Int Delay, s/veh

| Int Delay, s/veh | 2.7 | | | | | | | | |
|------------------------|------|------|------|------|------|------|--|--|---|
| Movement | EBL | EBR | NBL | NBT | SBT | SBR | | | ĺ |
| Lane Configurations | 1 | 1 | ۲. | 1 | ef – | | | | |
| Traffic Vol, veh/h | 98 | 34 | 23 | 174 | 449 | 93 | | | |
| Future Vol, veh/h | 98 | 34 | 23 | 174 | 449 | 93 | | | |
| Conflicting Peds, #/hr | 0 | 0 | 0 | 0 | 0 | 0 | | | |
| Sign Control | Stop | Stop | Free | Free | Free | Free | | | |
| RT Channelized | - | None | - | None | - | None | | | |
| Storage Length | 100 | 0 | 80 | - | - | - | | | |
| Veh in Median Storage, | # 0 | - | - | 0 | 0 | - | | | |
| Grade, % | 0 | - | - | 0 | 0 | - | | | |
| Peak Hour Factor | 98 | 98 | 98 | 98 | 98 | 98 | | | |
| Heavy Vehicles, % | 3 | 3 | 9 | 5 | 3 | 1 | | | |
| Mvmt Flow | 100 | 35 | 23 | 178 | 458 | 95 | | | |
| | | | | | | | | | |

| Major/Minor | Minor2 | | Major1 | Maj | or2 | | |
|----------------------|--------|-------|--------|-----|-----|---|--|
| Conflicting Flow All | 730 | 506 | 553 | 0 | - | 0 | |
| Stage 1 | 506 | - | - | - | - | - | |
| Stage 2 | 224 | - | - | - | - | - | |
| Critical Hdwy | 6.43 | 6.23 | 4.19 | - | - | - | |
| Critical Hdwy Stg 1 | 5.43 | - | - | - | - | - | |
| Critical Hdwy Stg 2 | 5.43 | - | - | - | - | - | |
| Follow-up Hdwy | 3.527 | 3.327 | 2.281 | - | - | - | |
| Pot Cap-1 Maneuver | 388 | 565 | 983 | - | - | - | |
| Stage 1 | 604 | - | - | - | - | - | |
| Stage 2 | 810 | - | - | - | - | - | |
| Platoon blocked, % | | | | - | - | - | |
| Mov Cap-1 Maneuver | 379 | 565 | 983 | - | - | - | |
| Mov Cap-2 Maneuver | 379 | - | - | - | - | - | |
| Stage 1 | 589 | - | - | - | - | - | |
| Stage 2 | 810 | - | - | - | - | - | |
| | | | | | | | |

| Approach | EB | NB | SB |
|--------------------|----------|------|----|
| HCM Control Delay, | s/v16.32 | 1.02 | 0 |
| HCM LOS | С | | |

| Minor Lane/Major Mvmt | NBL | NBT EBLn1 | EBLn2 | SBT | SBR | |
|---------------------------|-------|-----------|-------|-----|-----|--|
| Capacity (veh/h) | 983 | - 379 | 565 | - | - | |
| HCM Lane V/C Ratio | 0.024 | - 0.264 | 0.061 | - | - | |
| HCM Control Delay (s/veh) | 8.8 | - 17.9 | 11.8 | - | - | |
| HCM Lane LOS | А | - C | В | - | - | |
| HCM 95th %tile Q(veh) | 0.1 | - 1 | 0.2 | - | - | |

Int Delay, s/veh

| Int Delay, s/veh | 0.7 | | | | | | | |
|------------------------|------|------|------|------|------|------|--|--|
| Movement | EBL | EBR | NBL | NBT | SBT | SBR | | |
| Lane Configurations | ٦ | 1 | ٦ | 1 | ef 👘 | | | |
| Traffic Vol, veh/h | 10 | 22 | 10 | 198 | 480 | 10 | | |
| Future Vol, veh/h | 10 | 22 | 10 | 198 | 480 | 10 | | |
| Conflicting Peds, #/hr | 0 | 0 | 0 | 0 | 0 | 0 | | |
| Sign Control | Stop | Stop | Free | Free | Free | Free | | |
| RT Channelized | - | None | - | None | - | None | | |
| Storage Length | 100 | 0 | 115 | - | - | - | | |
| Veh in Median Storage | ,#0 | - | - | 0 | 0 | - | | |
| Grade, % | 0 | - | - | 0 | 0 | - | | |
| Peak Hour Factor | 92 | 92 | 92 | 92 | 92 | 92 | | |
| Heavy Vehicles, % | 1 | 9 | 1 | 6 | 3 | 1 | | |
| Mvmt Flow | 11 | 24 | 11 | 215 | 522 | 11 | | |

| Major/Minor | Minor2 | | Major1 | Maj | or2 | | |
|----------------------|--------|-------|--------|-----|-----|---|--|
| Conflicting Flow All | 764 | 527 | 533 | 0 | - | 0 | |
| Stage 1 | 527 | - | - | - | - | - | |
| Stage 2 | 237 | - | - | - | - | - | |
| Critical Hdwy | 6.41 | 6.29 | 4.11 | - | - | - | |
| Critical Hdwy Stg 1 | 5.41 | - | - | - | - | - | |
| Critical Hdwy Stg 2 | 5.41 | - | - | - | - | - | |
| Follow-up Hdwy | 3.509 | 3.381 | 2.209 | - | - | - | |
| Pot Cap-1 Maneuver | 373 | 537 | 1040 | - | - | - | |
| Stage 1 | 594 | - | - | - | - | - | |
| Stage 2 | 805 | - | - | - | - | - | |
| Platoon blocked, % | | | | - | - | - | |
| Mov Cap-1 Maneuver | 369 | 537 | 1040 | - | - | - | |
| Mov Cap-2 Maneuver | 369 | - | - | - | - | - | |
| Stage 1 | 588 | - | - | - | - | - | |
| Stage 2 | 805 | - | - | - | - | - | |
| | | | | | | | |

| Approach | EB | NB | SB |
|-------------------|-------------|------|----|
| HCM Control Delay | y, s/v12.96 | 0.41 | 0 |
| HCM LOS | В | | |

| Minor Lane/Major Mvmt | NBL | NBT EBLn ² | EBLn2 | SBT | SBR | |
|---------------------------|------|-----------------------|-------|-----|-----|--|
| Capacity (veh/h) | 1040 | - 369 | 537 | - | - | |
| HCM Lane V/C Ratio | 0.01 | - 0.029 | 0.044 | - | - | |
| HCM Control Delay (s/veh) | 8.5 | - 1 | 5 12 | - | - | |
| HCM Lane LOS | А | - (| ; В | - | - | |
| HCM 95th %tile Q(veh) | 0 | - 0.1 | 0.1 | - | - | |

Int Delay s/veh

| Movement WBL WBR NBT NBR SBL SBT Lane Configurations Y Image: Second Seco | Int Delay, s/veh | 2.6 | | | | | | | | | | | |
|---|------------------------|------|------|------|------|------|------|--|--|--|--|--|--|
| Lane Configurations Y Image: Configuration of the system Traffic Vol, veh/h 26 67 138 49 110 385 Future Vol, veh/h 26 67 138 49 110 385 Conflicting Peds, #/hr 0 0 0 0 0 0 Sign Control Stop Stop Free Free Free Free RT Channelized - None - None - None Storage Length 0 - 0 - 0 - 0 Grade, % 0 - 0 - 0 - 0 Peak Hour Factor 94 94 94 94 94 94 94 Heavy Vehicles, % 4 9 4 1 4 3 Mvmt Flow 28 71 147 52 117 410 | Movement | WBL | WBR | NBT | NBR | SBL | SBT | | | | | | |
| Traffic Vol, veh/h 26 67 138 49 110 385 Future Vol, veh/h 26 67 138 49 110 385 Conflicting Peds, #/hr 0 0 0 0 0 0 Sign Control Stop Stop Free Free Free Free RT Channelized - None - None - None Storage Length 0 - 0 - 0 - Veh in Median Storage, # 0 - 0 - 0 Grade, % 0 - 0 - 0 Peak Hour Factor 94 94 94 94 94 Heavy Vehicles, % 4 9 4 1 4 3 Mvmt Flow 28 71 147 52 117 410 | Lane Configurations | ۰¥ | | 4 | | | र्स | | | | | | |
| Future Vol, veh/h 26 67 138 49 110 385 Conflicting Peds, #/hr 0 0 0 0 0 0 0 Sign Control Stop Stop Free Free Free Free RT Channelized - None - None - None Storage Length 0 - - - - Veh in Median Storage, # 0 - 0 - 0 Grade, % 0 - 0 - 0 Peak Hour Factor 94 94 94 94 94 Heavy Vehicles, % 4 9 4 1 4 3 Mvmt Flow 28 71 147 52 117 410 | Traffic Vol, veh/h | 26 | 67 | 138 | 49 | 110 | 385 | | | | | | |
| Conflicting Peds, #/hr 0 | Future Vol, veh/h | 26 | 67 | 138 | 49 | 110 | 385 | | | | | | |
| Sign ControlStopStopFreeFreeFreeFreeRT Channelized-None-None-NoneStorage Length0Veh in Median Storage, #0-0-0Grade, %0-0-0Peak Hour Factor9494949494Heavy Vehicles, %49414Mvmt Flow287114752117410 | Conflicting Peds, #/hr | 0 | 0 | 0 | 0 | 0 | 0 | | | | | | |
| RT Channelized - None - None Storage Length 0 - - - Veh in Median Storage, # 0 - 0 - Grade, % 0 - 0 - 0 Peak Hour Factor 94 94 94 94 94 Heavy Vehicles, % 4 9 4 1 4 3 Mvmt Flow 28 71 147 52 117 410 | Sign Control | Stop | Stop | Free | Free | Free | Free | | | | | | |
| Storage Length 0 - - - - - Veh in Median Storage, # 0 - 0 - 0 - 0 Grade, % 0 - 0 - - 0 - 0 Peak Hour Factor 94 94 94 94 94 94 94 Heavy Vehicles, % 4 9 4 1 4 3 Mvmt Flow 28 71 147 52 117 410 | RT Channelized | - | None | - | None | - | None | | | | | | |
| Veh in Median Storage, # 0 - 0 - - 0 Grade, % 0 - 0 - 0 Peak Hour Factor 94 94 94 94 Heavy Vehicles, % 4 9 4 1 4 3 Mvmt Flow 28 71 147 52 117 410 | Storage Length | 0 | - | - | - | - | - | | | | | | |
| Grade, % 0 - 0 - - 0 Peak Hour Factor 94 94 94 94 94 94 Heavy Vehicles, % 4 9 4 1 4 3 Mvmt Flow 28 71 147 52 117 410 | Veh in Median Storage, | ,# 0 | - | 0 | - | - | 0 | | | | | | |
| Peak Hour Factor 94 94 94 94 94 94 Heavy Vehicles, % 4 9 4 1 4 3 Mvmt Flow 28 71 147 52 117 410 | Grade, % | 0 | - | 0 | - | - | 0 | | | | | | |
| Heavy Vehicles, % 4 9 4 1 4 3 Mvmt Flow 28 71 147 52 117 410 | Peak Hour Factor | 94 | 94 | 94 | 94 | 94 | 94 | | | | | | |
| Mvmt Flow 28 71 147 52 117 410 | Heavy Vehicles, % | 4 | 9 | 4 | 1 | 4 | 3 | | | | | | |
| | Mvmt Flow | 28 | 71 | 147 | 52 | 117 | 410 | | | | | | |

| Major/Minor | Minor1 | Ν | /lajor1 | Μ | lajor2 | | |
|----------------------|--------|-------|---------|-----|--------|---|--|
| Conflicting Flow All | 816 | 173 | 0 | 0 | 199 | 0 | |
| Stage 1 | 173 | - | - | - | - | - | |
| Stage 2 | 644 | - | - | - | - | - | |
| Critical Hdwy | 6.44 | 6.29 | - | - | 4.14 | - | |
| Critical Hdwy Stg 1 | 5.44 | - | - | - | - | - | |
| Critical Hdwy Stg 2 | 5.44 | - | - | - | - | - | |
| Follow-up Hdwy | 3.536 | 3.381 | - | - 2 | 2.236 | - | |
| Pot Cap-1 Maneuver | 344 | 853 | - | - | 1362 | - | |
| Stage 1 | 852 | - | - | - | - | - | |
| Stage 2 | 519 | - | - | - | - | - | |
| Platoon blocked, % | | | - | - | | - | |
| Mov Cap-1 Maneuver | 305 | 853 | - | - | 1362 | - | |
| Mov Cap-2 Maneuver | 305 | - | - | - | - | - | |
| Stage 1 | 852 | - | - | - | - | - | |
| Stage 2 | 462 | - | - | - | - | - | |
| | | | | | | | |

| Approach | WB | NB | SB |
|--------------------|----------|----|------|
| HCM Control Delay, | s/v12.67 | 0 | 1.75 |
| HCMLOS | В | | |

| Minor Lane/Major Mvmt | NBT | NBRWBLn1 | SBL | SBT | |
|---------------------------|-----|----------|-------|-----|--|
| Capacity (veh/h) | - | - 568 | 1362 | - | |
| HCM Lane V/C Ratio | - | - 0.174 | 0.086 | - | |
| HCM Control Delay (s/veh) | - | - 12.7 | 7.9 | 0 | |
| HCM Lane LOS | - | - E | A | А | |
| HCM 95th %tile Q(veh) | - | - 0.6 | 0.3 | - | |

Intersection Intersection Delay, s/veh Intersection LOS 11.6 В

| Movement | EBL | EBT | EBR | WBL | WBT | WBR | NBL | NBT | NBR | SBL | SBT | SBR |
|----------------------------|------|------|------|------|------|------|------|------|------|------|------|------|
| Lane Configurations | | 4 | | | \$ | | | \$ | | | \$ | |
| Traffic Vol, veh/h | 35 | 15 | 20 | 6 | 57 | 182 | 2 | 4 | 0 | 218 | 107 | 75 |
| Future Vol, veh/h | 35 | 15 | 20 | 6 | 57 | 182 | 2 | 4 | 0 | 218 | 107 | 75 |
| Peak Hour Factor | 0.97 | 0.97 | 0.97 | 0.97 | 0.97 | 0.97 | 0.97 | 0.97 | 0.97 | 0.97 | 0.97 | 0.97 |
| Heavy Vehicles, % | 3 | 20 | 1 | 1 | 2 | 3 | 1 | 25 | 1 | 2 | 1 | 8 |
| Mvmt Flow | 36 | 15 | 21 | 6 | 59 | 188 | 2 | 4 | 0 | 225 | 110 | 77 |
| Number of Lanes | 0 | 1 | 0 | 0 | 1 | 0 | 0 | 1 | 0 | 0 | 1 | 0 |
| Approach | EB | | | WB | | | NB | | | SB | | |
| Opposing Approach | WB | | | EB | | | SB | | | NB | | |
| Opposing Lanes | 1 | | | 1 | | | 1 | | | 1 | | |
| Conflicting Approach Left | SB | | | NB | | | EB | | | WB | | |
| Conflicting Lanes Left | 1 | | | 1 | | | 1 | | | 1 | | |
| Conflicting Approach Right | NB | | | SB | | | WB | | | EB | | |
| Conflicting Lanes Right | 1 | | | 1 | | | 1 | | | 1 | | |
| HCM Control Delay, s/veh | 8.9 | | | 9.9 | | | 8.4 | | | 13.2 | | |
| HCM LOS | А | | | А | | | А | | | В | | |

| Lane | NBLn1 | EBLn1 | WBLn1 | SBLn1 |
|--------------------------|-------|-------|-------|-------|
| Vol Left, % | 33% | 50% | 2% | 55% |
| Vol Thru, % | 67% | 21% | 23% | 27% |
| Vol Right, % | 0% | 29% | 74% | 19% |
| Sign Control | Stop | Stop | Stop | Stop |
| Traffic Vol by Lane | 6 | 70 | 245 | 400 |
| LT Vol | 2 | 35 | 6 | 218 |
| Through Vol | 4 | 15 | 57 | 107 |
| RT Vol | 0 | 20 | 182 | 75 |
| Lane Flow Rate | 6 | 72 | 253 | 412 |
| Geometry Grp | 1 | 1 | 1 | 1 |
| Degree of Util (X) | 0.009 | 0.105 | 0.323 | 0.538 |
| Departure Headway (Hd) | 5.273 | 5.22 | 4.597 | 4.695 |
| Convergence, Y/N | Yes | Yes | Yes | Yes |
| Сар | 671 | 681 | 778 | 763 |
| Service Time | 3.366 | 3.296 | 2.653 | 2.756 |
| HCM Lane V/C Ratio | 0.009 | 0.106 | 0.325 | 0.54 |
| HCM Control Delay, s/veh | 8.4 | 8.9 | 9.9 | 13.2 |
| HCM Lane LOS | A | А | А | В |
| HCM 95th-tile Q | 0 | 0.4 | 1.4 | 3.3 |

₩ Site: 7 [3. E Scott Ave & Lewis River Road (Site Folder: General)]

Output produced by SIDRA INTERSECTION Version: 9.1.3.210

Existing 2023 PM Peak Hour Site Category: (None) Roundabout

| Vehic | le Mo | ovement | Perfor | man | се | | | | | | | | | | |
|-----------|--------|--------------|-------------------------------|---------------------------|--------------------------------|--------------------------|---------------------|-----------------------|---------------------|------------------------------|--------------------------------|--------------|----------------------|---------------------------|-----------------------|
| Mov ID | Turn | Mov Class | Dem Fl [Total veh/h | nand Iows HV] % | Ar Fl [Total] veh/h | rival ows HV] % | Deg. Satn v/c | Aver. Delay sec | Level of Service | 95% E Qu [Veh. veh | Back Of eue Dist] ft | Prop. Que | Eff. Stop Rate | Aver. No. of Cycles | Aver. Speed mph |
| South: | Lewi | s River R | oad | | | | | | | | | | | | |
| 3 | L2 | All MCs | 65 | 1.6 | 65 | 1.6 | 0.613 | 11.7 | LOS B | 5.4 | 136.4 | 0.65 | 0.55 | 0.65 | 34.2 |
| 18a | R1 | All MCs | 669 | 1.0 | 669 | 1.0 | 0.613 | 5.0 | LOS A | 5.4 | 136.4 | 0.65 | 0.55 | 0.65 | 35.0 |
| Appro | ach | | 733 | 1.1 | 733 | 1.1 | 0.613 | 5.6 | LOS A | 5.4 | 136.4 | 0.65 | 0.55 | 0.65 | 34.9 |
| NorthE | ast: L | ewis Rive | er Road | | | | | | | | | | | | |
| 1ax | L1 | All MCs | 346 | 1.2 | 346 | 1.2 | 0.355 | 9.0 | LOS A | 2.6 | 64.5 | 0.28 | 0.53 | 0.28 | 33.7 |
| 16ax | R1 | All MCs | 139 | 1.0 | 139 | 1.0 | 0.355 | 3.5 | LOS A | 2.6 | 64.5 | 0.28 | 0.53 | 0.28 | 34.5 |
| Approa | ach | | 484 | 1.1 | 484 | 1.1 | 0.355 | 7.4 | LOS A | 2.6 | 64.5 | 0.28 | 0.53 | 0.28 | 33.9 |
| West: | E Sco | ott Avenue | • | | | | | | | | | | | | |
| 5a | L1 | All MCs | 233 | 1.0 | 233 | 1.0 | 0.236 | 10.4 | LOS B | 1.4 | 35.4 | 0.53 | 0.64 | 0.53 | 32.6 |
| 12 | R2 | All MCs | 26 | 1.0 | 26 | 1.0 | 0.236 | 5.5 | LOS A | 1.4 | 35.4 | 0.53 | 0.64 | 0.53 | 33.0 |
| Appro | ach | | 259 | 1.0 | 259 | 1.0 | 0.236 | 9.9 | LOS A | 1.4 | 35.4 | 0.53 | 0.64 | 0.53 | 32.7 |
| All Vel | nicles | | 1477 | 1.1 | 1477 | 1.1 | 0.613 | 6.9 | LOS A | 5.4 | 136.4 | 0.51 | 0.56 | 0.51 | 34.2 |

Site Level of Service (LOS) Method: Delay & Degree of Saturation (SIDRA). Site LOS Method is specified in the Parameter Settings dialog (Options tab).

Roundabout LOS Method: Same as Signalised Intersections.

Vehicle movement LOS values are based on average delay and v/c ratio (degree of saturation) per movement.

Intersection and Approach LOS values are based on average delay for all movements (v/c not used).

Roundabout Capacity Model: SIDRA HCM.

Delay Model: SIDRA Standard (Control Delay: Geometric Delay is included).

Queue Model: SIDRA queue estimation methods are used for Back of Queue and Queue at Start of Gap.

Gap-Acceptance Capacity Formula: SIDRA Standard (Akçelik M3D).

HV (%) values are calculated for All Movement Classes of All Heavy Vehicle Model Designation.

Arrival Flows used in performance calculations are adjusted to include any Initial Queued Demand and Upstream Capacity Constraint effects.

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SITE LAYOUT V Site: 7 [3. E Scott Ave & Lewis River Road (Site Folder: General)]

Existing 2023 PM Peak Hour Site Category: (None) Roundabout

Layout pictures are schematic functional drawings reflecting input data. They are not design drawings.



₩ Site: 1 [1. I-5 SB Ramps & Dike Access Road (Site Folder: Forecast 2026 Without Project)]

Output produced by SIDRA INTERSECTION Version: 9.1.3.210

Existing 2023 PM Peak Hour Site Category: (None) Roundabout

| Vehic | cle Mo | ovement | Perfor | man | се | | | | | | | | | | |
|-----------|----------|--------------|------------------------------|---------------------------|------------------------------|---------------------------|---------------------|-----------------------|---------------------|------------------------------|---------------------------------|--------------|----------------------|---------------------------|-----------------------|
| Mov ID | Turn | Mov Class | Dem F [Total veh/h | nand Iows HV] % | Ar Fl [Total veh/h | rival lows HV] % | Deg. Satn v/c | Aver. Delay sec | Level of Service | 95% I Qu [Veh. veh | Back Of Jeue Dist] ft | Prop. Que | Eff. Stop Rate | Aver. No. of Cycles | Aver. Speed mph |
| East: | Dike A | ccess Ro | ad | | | | | | | | | | | | |
| 1 | L2 | All MCs | 124 | 5.1 | 124 | 5.1 | 0.366 | 9.8 | LOS A | 0.0 | 0.0 | 0.00 | 0.48 | 0.00 | 35.1 |
| 6 | T1 | All MCs | 385 | 3.3 | 385 | 3.3 | 0.366 | 3.8 | LOS A | 0.0 | 0.0 | 0.00 | 0.48 | 0.00 | 36.0 |
| Appro | ach | | 510 | 3.7 | 510 | 3.7 | 0.366 | 5.3 | LOS A | 0.0 | 0.0 | 0.00 | 0.48 | 0.00 | 35.8 |
| North | : I-5 SI | 3 Off-Ram | ıp | | | | | | | | | | | | |
| 7 | L2 | All MCs | 177 | 9.7 | 177 | 9.7 | 0.437 | 14.2 | LOS B | 2.8 | 73.7 | 0.70 | 0.70 | 0.71 | 32.3 |
| 4 | T1 | All MCs | 5 | 1.0 | 5 | 1.0 | 0.437 | 7.5 | LOS A | 2.8 | 73.7 | 0.70 | 0.70 | 0.71 | 33.2 |
| 14 | R2 | All MCs | 209 | 3.3 | 209 | 3.3 | 0.437 | 7.8 | LOS A | 2.8 | 73.7 | 0.70 | 0.70 | 0.71 | 32.9 |
| Appro | ach | | 390 | 6.2 | 390 | 6.2 | 0.437 | 10.7 | LOS B | 2.8 | 73.7 | 0.70 | 0.70 | 0.71 | 32.6 |
| West: | Dike / | Access Ro | bad | | | | | | | | | | | | |
| 2 | T1 | All MCs | 604 | 1.0 | 604 | 1.0 | 0.804 | 10.9 | LOS B | 12.7 | 320.7 | 0.93 | 0.83 | 1.20 | 33.0 |
| 12 | R2 | All MCs | 261 | 2.6 | 261 | 2.6 | 0.804 | 11.1 | LOS B | 12.7 | 320.7 | 0.93 | 0.83 | 1.20 | 32.7 |
| Appro | ach | | 865 | 1.5 | 865 | 1.5 | 0.804 | 11.0 | LOS B | 12.7 | 320.7 | 0.93 | 0.83 | 1.20 | 32.9 |
| All Ve | hicles | | 1765 | 3.2 | 1765 | 3.2 | 0.804 | 9.3 | LOS A | 12.7 | 320.7 | 0.61 | 0.70 | 0.74 | 33.6 |

Site Level of Service (LOS) Method: Delay & Degree of Saturation (SIDRA). Site LOS Method is specified in the Parameter Settings dialog (Options tab).

Roundabout LOS Method: Same as Signalised Intersections.

Vehicle movement LOS values are based on average delay and v/c ratio (degree of saturation) per movement.

Intersection and Approach LOS values are based on average delay for all movements (v/c not used).

Roundabout Capacity Model: SIDRA HCM.

Delay Model: SIDRA Standard (Control Delay: Geometric Delay is included).

Queue Model: SIDRA queue estimation methods are used for Back of Queue and Queue at Start of Gap.

Gap-Acceptance Capacity Formula: SIDRA Standard (Akçelik M3D).

HV (%) values are calculated for All Movement Classes of All Heavy Vehicle Model Designation.

Arrival Flows used in performance calculations are adjusted to include any Initial Queued Demand and Upstream Capacity Constraint effects.

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Project: C:\Users\pwhalen\Heath and Associates\Canon Scans - Documents\Logan's Landing\LOS 2023\2. Forecast 2026 Without Project.sip9

V Site: 2 [2. I-5 NB Ramp & Dike Access Road (Site Folder: Forecast 2026 Without Project)]

Output produced by SIDRA INTERSECTION Version: 9.1.3.210

Exsiting 2023 PM Peak Hour Site Category: (None) Roundabout

| Vehic | le Mo | ovement | Perfor | man | се | | | | | | | | | | |
|-----------|---------|--------------|------------------------------|---------------------------|------------------------------|----------------------------|---------------------|-----------------------|---------------------|---------------------------|---------------------------------|--------------|----------------------|---------------------------|-----------------------|
| Mov ID | Turn | Mov Class | Den F [Total veh/h | nand lows HV] % | Ar F∣ [Total veh/h | rival lows HV] % | Deg. Satn v/c | Aver. Delay sec | Level of Service | 95% Q [Veh. veh | Back Of ueue Dist] ft | Prop. Que | Eff. Stop Rate | Aver. No. of Cycles | Aver. Speed mph |
| South | : I-5 N | B Off-Rar | np | | | | | | | | | | | | |
| 3 | L2 | All MCs | 224 | 5.6 | 224 | 5.6 | 0.477 | 19.9 | LOS B | 3.7 | 96.7 | 0.86 | 0.87 | 1.06 | 29.4 |
| 8 | T1 | All MCs | 1 | 1.0 | 1 | 1.0 | 0.477 | 13.2 | LOS B | 3.7 | 96.7 | 0.86 | 0.87 | 1.06 | 30.0 |
| 18 | R2 | All MCs | 96 | 4.4 | 96 | 4.4 | 0.477 | 13.8 | LOS B | 3.7 | 96.7 | 0.86 | 0.87 | 1.06 | 29.7 |
| Appro | ach | | 321 | 5.2 | 321 | 5.2 | 0.477 | 18.1 | LOS B | 3.7 | 96.7 | 0.86 | 0.87 | 1.06 | 29.5 |
| East: | Dike A | ccess Ro | ad | | | | | | | | | | | | |
| 6 | T1 | All MCs | 254 | 3.8 | 254 | 3.8 | 0.410 | 7.8 | LOS A | 2.8 | 71.5 | 0.76 | 0.67 | 0.76 | 34.3 |
| 16 | R2 | All MCs | 89 | 5.6 | 89 | 5.6 | 0.410 | 8.1 | LOS A | 2.8 | 71.5 | 0.76 | 0.67 | 0.76 | 33.9 |
| Appro | ach | | 344 | 4.3 | 344 | 4.3 | 0.410 | 7.9 | LOS A | 2.8 | 71.5 | 0.76 | 0.67 | 0.76 | 34.2 |
| West: | Dike / | Access Ro | bad | | | | | | | | | | | | |
| 5 | L2 | All MCs | 332 | 3.1 | 332 | 3.1 | 0.623 | 9.7 | LOS A | 0.0 | 0.0 | 0.00 | 0.52 | 0.00 | 34.8 |
| 2 | T1 | All MCs | 541 | 2.8 | 541 | 2.8 | 0.623 | 3.7 | LOS A | 0.0 | 0.0 | 0.00 | 0.52 | 0.00 | 35.6 |
| Appro | ach | | 873 | 2.9 | 873 | 2.9 | 0.623 | 6.0 | LOS A | 0.0 | 0.0 | 0.00 | 0.52 | 0.00 | 35.3 |
| All Vel | hicles | | 1538 | 3.7 | 1538 | 3.7 | 0.623 | 9.0 | LOS A | 3.7 | 96.7 | 0.35 | 0.63 | 0.39 | 33.6 |

Site Level of Service (LOS) Method: Delay & Degree of Saturation (SIDRA). Site LOS Method is specified in the Parameter Settings dialog (Options tab).

Roundabout LOS Method: Same as Signalised Intersections.

Vehicle movement LOS values are based on average delay and v/c ratio (degree of saturation) per movement.

Intersection and Approach LOS values are based on average delay for all movements (v/c not used).

Roundabout Capacity Model: SIDRA HCM.

Delay Model: SIDRA Standard (Control Delay: Geometric Delay is included).

Queue Model: SIDRA queue estimation methods are used for Back of Queue and Queue at Start of Gap.

Gap-Acceptance Capacity Formula: SIDRA Standard (Akçelik M3D).

HV (%) values are calculated for All Movement Classes of All Heavy Vehicle Model Designation.

Arrival Flows used in performance calculations are adjusted to include any Initial Queued Demand and Upstream Capacity Constraint effects.

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Int Delay, s/veh

| Int Delay, s/veh | 3 | | | | | | |
|------------------------|------|------|------|------|------|------|--|
| Movement | EBL | EBR | NBL | NBT | SBT | SBR | |
| Lane Configurations | 1 | 1 | ۲. | 1 | ef – | | |
| Traffic Vol, veh/h | 105 | 36 | 25 | 210 | 517 | 100 | |
| Future Vol, veh/h | 105 | 36 | 25 | 210 | 517 | 100 | |
| Conflicting Peds, #/hr | 0 | 0 | 0 | 0 | 0 | 0 | |
| Sign Control | Stop | Stop | Free | Free | Free | Free | |
| RT Channelized | - | None | - | None | - | None | |
| Storage Length | 100 | 0 | 80 | - | - | - | |
| Veh in Median Storage, | # 0 | - | - | 0 | 0 | - | |
| Grade, % | 0 | - | - | 0 | 0 | - | |
| Peak Hour Factor | 98 | 98 | 98 | 98 | 98 | 98 | |
| Heavy Vehicles, % | 3 | 3 | 9 | 5 | 3 | 1 | |
| Mvmt Flow | 107 | 37 | 26 | 214 | 528 | 102 | |
| | | | | | | | |

| Major/Minor | Minor2 | l | Major1 | Ma | jor2 | |
|----------------------|--------|-------|--------|----|------|---|
| Conflicting Flow All | 844 | 579 | 630 | 0 | - | 0 |
| Stage 1 | 579 | - | - | - | - | - |
| Stage 2 | 265 | - | - | - | - | - |
| Critical Hdwy | 6.43 | 6.23 | 4.19 | - | - | - |
| Critical Hdwy Stg 1 | 5.43 | - | - | - | - | - |
| Critical Hdwy Stg 2 | 5.43 | - | - | - | - | - |
| Follow-up Hdwy | 3.527 | 3.327 | 2.281 | - | - | - |
| Pot Cap-1 Maneuver | 332 | 513 | 920 | - | - | - |
| Stage 1 | 559 | - | - | - | - | - |
| Stage 2 | 777 | - | - | - | - | - |
| Platoon blocked, % | | | | - | - | - |
| Mov Cap-1 Maneuver | 323 | 513 | 920 | - | - | - |
| Mov Cap-2 Maneuver | 323 | - | - | - | - | - |
| Stage 1 | 543 | - | - | - | - | - |
| Stage 2 | 777 | - | - | - | - | - |
| | | | | | | |

| Approach | EB | NB | SB |
|-------------------|-------------|------|----|
| HCM Control Delay | y, s/v19.27 | 0.96 | 0 |
| HCM LOS | С | | |

| Minor Lane/Major Mvmt | NBL | NBT EBLn1 | EBLn2 | SBT | SBR | |
|---------------------------|-------|-----------|-------|-----|-----|--|
| Capacity (veh/h) | 920 | - 323 | 513 | - | - | |
| HCM Lane V/C Ratio | 0.028 | - 0.332 | 0.072 | - | - | |
| HCM Control Delay (s/veh) | 9 | - 21.6 | 12.6 | - | - | |
| HCM Lane LOS | А | - C | В | - | - | |
| HCM 95th %tile Q(veh) | 0.1 | - 1.4 | 0.2 | - | - | |

| Int Delay, s/veh | 0.7 | | | | | |
|------------------------|------|------|------|------|------|------|
| Movement | EBL | EBR | NBL | NBT | SBT | SBR |
| Lane Configurations | ٢ | 1 | 1 | 1 | ef – | |
| Traffic Vol, veh/h | 11 | 24 | 11 | 236 | 550 | 11 |
| Future Vol, veh/h | 11 | 24 | 11 | 236 | 550 | 11 |
| Conflicting Peds, #/hr | 0 | 0 | 0 | 0 | 0 | 0 |
| Sign Control | Stop | Stop | Free | Free | Free | Free |
| RT Channelized | - | None | - | None | - | None |
| Storage Length | 100 | 0 | 115 | - | - | - |
| Veh in Median Storage | ,# 0 | - | - | 0 | 0 | - |
| Grade, % | 0 | - | - | 0 | 0 | - |
| Peak Hour Factor | 92 | 92 | 92 | 92 | 92 | 92 |
| Heavy Vehicles, % | 1 | 9 | 1 | 6 | 3 | 1 |
| Mvmt Flow | 12 | 26 | 12 | 257 | 598 | 12 |

| Major/Minor | Minor2 | | Major1 | Ма | jor2 | |
|----------------------|--------|-------|--------|----|------|---|
| Conflicting Flow All | 884 | 604 | 610 | 0 | - | 0 |
| Stage 1 | 604 | - | - | - | - | - |
| Stage 2 | 280 | - | - | - | - | - |
| Critical Hdwy | 6.41 | 6.29 | 4.11 | - | - | - |
| Critical Hdwy Stg 1 | 5.41 | - | - | - | - | - |
| Critical Hdwy Stg 2 | 5.41 | - | - | - | - | - |
| Follow-up Hdwy | 3.509 | 3.381 | 2.209 | - | - | - |
| Pot Cap-1 Maneuver | 317 | 486 | 974 | - | - | - |
| Stage 1 | 548 | - | - | - | - | - |
| Stage 2 | 769 | - | - | - | - | - |
| Platoon blocked, % | | | | - | - | - |
| Mov Cap-1 Maneuver | 313 | 486 | 974 | - | - | - |
| Mov Cap-2 Maneuver | 313 | - | - | - | - | - |
| Stage 1 | 541 | - | - | - | - | - |
| Stage 2 | 769 | - | - | - | - | - |
| | | | | | | |

| Approach | EB | NB | SB |
|-------------------|-------------|------|----|
| HCM Control Delay | v, s/v14.13 | 0.39 | 0 |
| HCM LOS | В | | |

| Minor Lane/Major Mvmt | NBL | NBT EBL | 1 EBLn2 | SBT | SBR | |
|---------------------------|-------|---------|----------|-----|-----|--|
| Capacity (veh/h) | 974 | - 3 | 13 486 | - | - | |
| HCM Lane V/C Ratio | 0.012 | - 0.0 | 88 0.054 | - | - | |
| HCM Control Delay (s/veh) | 8.7 | - | 12.8 | - | - | |
| HCM Lane LOS | A | - | C B | - | - | |
| HCM 95th %tile Q(veh) | 0 | - 0 | .1 0.2 | - | - | |

Int Delay s/yeh

| Int Delay, siven 5.5 | | | | | | | | |
|----------------------------|------|------|------|------|------|--|--|--|
| Movement WBL | WBR | NBT | NBR | SBL | SBT | | | |
| Lane Configurations | | ef 👘 | | | ्स | | | |
| Traffic Vol, veh/h 35 | 96 | 148 | 65 | 154 | 412 | | | |
| Future Vol, veh/h 35 | 96 | 148 | 65 | 154 | 412 | | | |
| Conflicting Peds, #/hr 0 | 0 | 0 | 0 | 0 | 0 | | | |
| Sign Control Stop | Stop | Free | Free | Free | Free | | | |
| RT Channelized - | None | - | None | - | None | | | |
| Storage Length 0 | - | - | - | - | - | | | |
| Veh in Median Storage, # 0 | - | 0 | - | - | 0 | | | |
| Grade, % 0 | - | 0 | - | - | 0 | | | |
| Peak Hour Factor 94 | 94 | 94 | 94 | 94 | 94 | | | |
| Heavy Vehicles, % 4 | 9 | 4 | 1 | 4 | 3 | | | |
| Mvmt Flow 37 | 102 | 157 | 69 | 164 | 438 | | | |

| Major/Minor | Minor1 | Ν | 1ajor1 | Ν | lajor2 | |
|----------------------|--------|-------|--------|---|--------|---|
| Conflicting Flow All | 958 | 192 | 0 | 0 | 227 | 0 |
| Stage 1 | 192 | - | - | - | - | - |
| Stage 2 | 766 | - | - | - | - | - |
| Critical Hdwy | 6.44 | 6.29 | - | - | 4.14 | - |
| Critical Hdwy Stg 1 | 5.44 | - | - | - | - | - |
| Critical Hdwy Stg 2 | 5.44 | - | - | - | - | - |
| Follow-up Hdwy | 3.536 | 3.381 | - | - | 2.236 | - |
| Pot Cap-1 Maneuver | 283 | 832 | - | - | 1330 | - |
| Stage 1 | 836 | - | - | - | - | - |
| Stage 2 | 455 | - | - | - | - | - |
| Platoon blocked, % | | | - | - | | - |
| Mov Cap-1 Maneuver | 237 | 832 | - | - | 1330 | - |
| Mov Cap-2 Maneuver | 237 | - | - | - | - | - |
| Stage 1 | 836 | - | - | - | - | - |
| Stage 2 | 381 | - | - | - | - | - |
| | | | | | | |

| Approach | WB | NB | SB |
|-------------------|-------------|----|-----|
| HCM Control Delay | /, s/v15.01 | 0 | 2.2 |
| HCM LOS | С | | |

| Minor Lane/Major Mvmt | NBT | NBRW | /BLn1 | SBL | SBT | |
|---------------------------|-----|------|-------|-------|-----|--|
| Capacity (veh/h) | - | - | 498 | 1330 | - | |
| HCM Lane V/C Ratio | - | - | 0.28 | 0.123 | - | |
| HCM Control Delay (s/veh) | - | - | 15 | 8.1 | 0 | |
| HCM Lane LOS | - | - | С | А | А | |
| HCM 95th %tile Q(veh) | - | - | 1.1 | 0.4 | - | |

Intersection Delay, s/veh 12.7

В

Intersection Delay, s/veh Intersection LOS

| Movement | EBL | EBT | EBR | WBL | WBT | WBR | NBL | NBT | NBR | SBL | SBT | SBR |
|----------------------------|------|------|------|------|------|------|------|------|------|------|------|------|
| Lane Configurations | | \$ | | | ÷ | | | \$ | | | \$ | |
| Traffic Vol, veh/h | 37 | 16 | 21 | 6 | 61 | 208 | 2 | 4 | 0 | 234 | 121 | 80 |
| Future Vol, veh/h | 37 | 16 | 21 | 6 | 61 | 208 | 2 | 4 | 0 | 234 | 121 | 80 |
| Peak Hour Factor | 0.97 | 0.97 | 0.97 | 0.97 | 0.97 | 0.97 | 0.97 | 0.97 | 0.97 | 0.97 | 0.97 | 0.97 |
| Heavy Vehicles, % | 3 | 20 | 1 | 1 | 2 | 3 | 1 | 25 | 1 | 2 | 1 | 8 |
| Mvmt Flow | 38 | 16 | 22 | 6 | 63 | 214 | 2 | 4 | 0 | 241 | 125 | 82 |
| Number of Lanes | 0 | 1 | 0 | 0 | 1 | 0 | 0 | 1 | 0 | 0 | 1 | 0 |
| Approach | EB | | | WB | | | NB | | | SB | | |
| Opposing Approach | WB | | | EB | | | SB | | | NB | | |
| Opposing Lanes | 1 | | | 1 | | | 1 | | | 1 | | |
| Conflicting Approach Left | SB | | | NB | | | EB | | | WB | | |
| Conflicting Lanes Left | 1 | | | 1 | | | 1 | | | 1 | | |
| Conflicting Approach Right | NB | | | SB | | | WB | | | EB | | |
| Conflicting Lanes Right | 1 | | | 1 | | | 1 | | | 1 | | |
| HCM Control Delay, s/veh | 9.2 | | | 10.5 | | | 8.6 | | | 14.8 | | |
| HCM LOS | А | | | В | | | А | | | В | | |

| Lane | NBLn1 | EBLn1 | WBLn1 | SBLn1 | |
|--------------------------|-------|-------|-------|-------|--|
| Vol Left, % | 33% | 50% | 2% | 54% | |
| Vol Thru, % | 67% | 22% | 22% | 28% | |
| Vol Right, % | 0% | 28% | 76% | 18% | |
| Sign Control | Stop | Stop | Stop | Stop | |
| Traffic Vol by Lane | 6 | 74 | 275 | 435 | |
| LT Vol | 2 | 37 | 6 | 234 | |
| Through Vol | 4 | 16 | 61 | 121 | |
| RT Vol | 0 | 21 | 208 | 80 | |
| Lane Flow Rate | 6 | 76 | 284 | 448 | |
| Geometry Grp | 1 | 1 | 1 | 1 | |
| Degree of Util (X) | 0.01 | 0.114 | 0.37 | 0.596 | |
| Departure Headway (Hd) | 5.551 | 5.376 | 4.701 | 4.787 | |
| Convergence, Y/N | Yes | Yes | Yes | Yes | |
| Сар | 649 | 659 | 760 | 749 | |
| Service Time | 3.551 | 3.472 | 2.772 | 2.862 | |
| HCM Lane V/C Ratio | 0.009 | 0.115 | 0.374 | 0.598 | |
| HCM Control Delay, s/veh | 8.6 | 9.2 | 10.5 | 14.8 | |
| HCM Lane LOS | A | А | В | В | |
| HCM 95th-tile Q | 0 | 0.4 | 1.7 | 4 | |

₩ Site: 7 [3. E Scott Ave & Lewis River Road (Site Folder: Forecast 2026 Without Project)]

Output produced by SIDRA INTERSECTION Version: 9.1.3.210

Existing 2023 PM Peak Hour Site Category: (None) Roundabout

| Vehic | le Mo | ovement | Perfor | man | ce | | | | | | | | | | |
|-----------|--------|--------------|-------------------------------|---------------------------|--------------------------------|--------------------------|---------------------|-----------------------|---------------------|------------------------------|-------------------------------|--------------|----------------------|---------------------------|-----------------------|
| Mov ID | Turn | Mov Class | Dem Fi [Total veh/h | nand lows HV] % | Ar Fl [Total] veh/h | rival ows HV] % | Deg. Satn v/c | Aver. Delay sec | Level of Service | 95% B Qu [Veh. veh | ack Of eue Dist] ft | Prop. Que | Eff. Stop Rate | Aver. No. of Cycles | Aver. Speed mph |
| South: | Lewi | s River R | oad | | | | | | | | | | | | |
| 3 | L2 | All MCs | 79 | 1.6 | 79 | 1.6 | 0.742 | 13.8 | LOS B | 9.4 | 238.0 | 0.81 | 0.67 | 0.91 | 33.6 |
| 18a | R1 | All MCs | 779 | 1.0 | 779 | 1.0 | 0.742 | 7.1 | LOS A | 9.4 | 238.0 | 0.81 | 0.67 | 0.91 | 34.4 |
| Approa | ach | | 858 | 1.1 | 858 | 1.1 | 0.742 | 7.7 | LOS A | 9.4 | 238.0 | 0.81 | 0.67 | 0.91 | 34.3 |
| NorthE | ast: L | ewis Rive | er Road | | | | | | | | | | | | |
| 1ax | L1 | All MCs | 407 | 1.2 | 407 | 1.2 | 0.423 | 9.1 | LOS A | 3.4 | 86.3 | 0.35 | 0.53 | 0.35 | 33.5 |
| 16ax | R1 | All MCs | 159 | 1.0 | 159 | 1.0 | 0.423 | 3.7 | LOS A | 3.4 | 86.3 | 0.35 | 0.53 | 0.35 | 34.3 |
| Approa | ach | | 567 | 1.1 | 567 | 1.1 | 0.423 | 7.6 | LOS A | 3.4 | 86.3 | 0.35 | 0.53 | 0.35 | 33.8 |
| West: | E Sco | ott Avenue | ; | | | | | | | | | | | | |
| 5a | L1 | All MCs | 266 | 1.0 | 266 | 1.0 | 0.283 | 10.9 | LOS B | 1.8 | 44.7 | 0.60 | 0.66 | 0.60 | 32.5 |
| 12 | R2 | All MCs | 28 | 1.0 | 28 | 1.0 | 0.283 | 6.0 | LOS A | 1.8 | 44.7 | 0.60 | 0.66 | 0.60 | 32.9 |
| Approa | ach | | 294 | 1.0 | 294 | 1.0 | 0.283 | 10.4 | LOS B | 1.8 | 44.7 | 0.60 | 0.66 | 0.60 | 32.5 |
| All Veh | nicles | | 1719 | 1.1 | 1719 | 1.1 | 0.742 | 8.1 | LOS A | 9.4 | 238.0 | 0.62 | 0.62 | 0.67 | 33.8 |

Site Level of Service (LOS) Method: Delay & Degree of Saturation (SIDRA). Site LOS Method is specified in the Parameter Settings dialog (Options tab).

Roundabout LOS Method: Same as Signalised Intersections.

Vehicle movement LOS values are based on average delay and v/c ratio (degree of saturation) per movement.

Intersection and Approach LOS values are based on average delay for all movements (v/c not used).

Roundabout Capacity Model: SIDRA HCM.

Delay Model: SIDRA Standard (Control Delay: Geometric Delay is included).

Queue Model: SIDRA queue estimation methods are used for Back of Queue and Queue at Start of Gap.

Gap-Acceptance Capacity Formula: SIDRA Standard (Akçelik M3D).

HV (%) values are calculated for All Movement Classes of All Heavy Vehicle Model Designation.

Arrival Flows used in performance calculations are adjusted to include any Initial Queued Demand and Upstream Capacity Constraint effects.

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Project: C:\Users\pwhalen\Heath and Associates\Canon Scans - Documents\Logan's Landing\LOS 2023\2. Forecast 2026 Without Project.sip9

₩ Site: 1 [1. I-5 SB Ramps & Dike Access Road (Site Folder: Forecast 2026 With Project)]

Output produced by SIDRA INTERSECTION Version: 9.1.3.210

Forecast 2026 PM Peak Hour With Project Site Category: (None) Roundabout

| Vehic | cle Mo | ovement | Perfor | man | се | | | | | | | | | | |
|-----------|----------|--------------|------------------------------|---------------------------|------------------------------|----------------------------|---------------------|-----------------------|---------------------|------------------------------|---------------------------------|--------------|----------------------|---------------------------|-----------------------|
| Mov ID | Turn | Mov Class | Dem F [Total veh/h | nand lows HV] % | Ar F∣ [Total veh/h | rival lows HV] % | Deg. Satn v/c | Aver. Delay sec | Level of Service | 95% I Qu [Veh. veh | Back Of Jeue Dist] ft | Prop. Que | Eff. Stop Rate | Aver. No. of Cycles | Aver. Speed mph |
| East: | Dike A | ccess Ro | ad | | | | | | | | | | | | |
| 1 | L2 | All MCs | 159 | 5.1 | 159 | 5.1 | 0.401 | 9.8 | LOS A | 0.0 | 0.0 | 0.00 | 0.49 | 0.00 | 35.0 |
| 6 | T1 | All MCs | 399 | 3.3 | 399 | 3.3 | 0.401 | 3.8 | LOS A | 0.0 | 0.0 | 0.00 | 0.49 | 0.00 | 35.9 |
| Appro | ach | | 557 | 3.8 | 557 | 3.8 | 0.401 | 5.5 | LOS A | 0.0 | 0.0 | 0.00 | 0.49 | 0.00 | 35.6 |
| North: | : I-5 SI | 3 Off-Ram | ıp | | | | | | | | | | | | |
| 7 | L2 | All MCs | 204 | 9.7 | 204 | 9.7 | 0.488 | 15.6 | LOS B | 3.6 | 93.5 | 0.75 | 0.76 | 0.84 | 31.6 |
| 4 | T1 | All MCs | 5 | 1.0 | 5 | 1.0 | 0.488 | 8.7 | LOS A | 3.6 | 93.5 | 0.75 | 0.76 | 0.84 | 32.5 |
| 14 | R2 | All MCs | 209 | 3.3 | 209 | 3.3 | 0.488 | 9.0 | LOS A | 3.6 | 93.5 | 0.75 | 0.76 | 0.84 | 32.2 |
| Appro | ach | | 418 | 6.4 | 418 | 6.4 | 0.488 | 12.2 | LOS B | 3.6 | 93.5 | 0.75 | 0.76 | 0.84 | 31.9 |
| West: | Dike / | Access Ro | bad | | | | | | | | | | | | |
| 2 | T1 | All MCs | 621 | 1.0 | 621 | 1.0 | 0.868 | 15.2 | LOS D | 16.8 | 424.6 | 1.00 | 1.03 | 1.52 | 31.0 |
| 12 | R2 | All MCs | 261 | 2.6 | 261 | 2.6 | 0.868 | 15.5 | LOS D | 16.8 | 424.6 | 1.00 | 1.03 | 1.52 | 30.7 |
| Appro | ach | | 882 | 1.5 | 882 | 1.5 | 0.868 | 15.3 | LOS B | 16.8 | 424.6 | 1.00 | 1.03 | 1.52 | 30.9 |
| All Ve | hicles | | 1857 | 3.3 | 1857 | 3.3 | 0.868 | 11.7 | LOS B | 16.8 | 424.6 | 0.64 | 0.81 | 0.91 | 32.4 |

Site Level of Service (LOS) Method: Delay & Degree of Saturation (SIDRA). Site LOS Method is specified in the Parameter Settings dialog (Options tab).

Roundabout LOS Method: Same as Signalised Intersections.

Vehicle movement LOS values are based on average delay and v/c ratio (degree of saturation) per movement.

Intersection and Approach LOS values are based on average delay for all movements (v/c not used).

Roundabout Capacity Model: SIDRA HCM.

Delay Model: SIDRA Standard (Control Delay: Geometric Delay is included).

Queue Model: SIDRA queue estimation methods are used for Back of Queue and Queue at Start of Gap.

Gap-Acceptance Capacity Formula: SIDRA Standard (Akçelik M3D).

HV (%) values are calculated for All Movement Classes of All Heavy Vehicle Model Designation.

Arrival Flows used in performance calculations are adjusted to include any Initial Queued Demand and Upstream Capacity Constraint effects.

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₩ Site: 2 [2. I-5 NB Ramp & Dike Access Road (Site Folder: Forecast 2026 With Project)]

Output produced by SIDRA INTERSECTION Version: 9.1.3.210

Forecast 2028 PM Peak Hour With Project Site Category: (None) Roundabout

| Vehic | le Mo | ovement | Perfor | man | се | | | | | | | | | | |
|-----------|---------|--------------|------------------------------|---------------------------|------------------------------|----------------------------|---------------------|-----------------------|---------------------|---------------------------|---------------------------------|--------------|----------------------|---------------------------|-----------------------|
| Mov ID | Turn | Mov Class | Dem F [Total veh/h | nand lows HV] % | Ar Fl [Total veh/h | rival lows HV] % | Deg. Satn v/c | Aver. Delay sec | Level of Service | 95% Q [Veh. veh | Back Of ueue Dist] ft | Prop. Que | Eff. Stop Rate | Aver. No. of Cycles | Aver. Speed mph |
| South | : I-5 N | B Off-Rar | np | | | | | | | | | | | | |
| 3 | L2 | All MCs | 224 | 5.6 | 224 | 5.6 | 0.556 | 23.1 | LOS C | 5.0 | 131.1 | 0.91 | 0.95 | 1.27 | 28.4 |
| 8 | T1 | All MCs | 1 | 1.0 | 1 | 1.0 | 0.556 | 16.3 | LOS B | 5.0 | 131.1 | 0.91 | 0.95 | 1.27 | 29.0 |
| 18 | R2 | All MCs | 134 | 4.4 | 134 | 4.4 | 0.556 | 17.0 | LOS B | 5.0 | 131.1 | 0.91 | 0.95 | 1.27 | 28.7 |
| Appro | ach | | 360 | 5.1 | 360 | 5.1 | 0.556 | 20.8 | LOS C | 5.0 | 131.1 | 0.91 | 0.95 | 1.27 | 28.5 |
| East: | Dike A | ccess Ro | ad | | | | | | | | | | | | |
| 6 | T1 | All MCs | 302 | 3.8 | 302 | 3.8 | 0.498 | 9.0 | LOS A | 4.0 | 102.2 | 0.80 | 0.73 | 0.89 | 33.9 |
| 16 | R2 | All MCs | 114 | 5.6 | 114 | 5.6 | 0.498 | 9.2 | LOS A | 4.0 | 102.2 | 0.80 | 0.73 | 0.89 | 33.5 |
| Appro | ach | | 416 | 4.3 | 416 | 4.3 | 0.498 | 9.0 | LOS A | 4.0 | 102.2 | 0.80 | 0.73 | 0.89 | 33.8 |
| West: | Dike / | Access Ro | oad | | | | | | | | | | | | |
| 5 | L2 | All MCs | 332 | 3.1 | 332 | 3.1 | 0.655 | 9.7 | LOS A | 0.0 | 0.0 | 0.00 | 0.52 | 0.00 | 34.8 |
| 2 | T1 | All MCs | 586 | 2.8 | 586 | 2.8 | 0.655 | 3.7 | LOS A | 0.0 | 0.0 | 0.00 | 0.52 | 0.00 | 35.6 |
| Appro | ach | | 918 | 2.9 | 918 | 2.9 | 0.655 | 5.9 | LOS A | 0.0 | 0.0 | 0.00 | 0.52 | 0.00 | 35.3 |
| All Vel | nicles | | 1694 | 3.7 | 1694 | 3.7 | 0.655 | 9.8 | LOS A | 5.0 | 131.1 | 0.39 | 0.66 | 0.49 | 33.3 |

Site Level of Service (LOS) Method: Delay & Degree of Saturation (SIDRA). Site LOS Method is specified in the Parameter Settings dialog (Options tab).

Roundabout LOS Method: Same as Signalised Intersections.

Vehicle movement LOS values are based on average delay and v/c ratio (degree of saturation) per movement.

Intersection and Approach LOS values are based on average delay for all movements (v/c not used).

Roundabout Capacity Model: SIDRA HCM.

Delay Model: SIDRA Standard (Control Delay: Geometric Delay is included).

Queue Model: SIDRA queue estimation methods are used for Back of Queue and Queue at Start of Gap.

Gap-Acceptance Capacity Formula: SIDRA Standard (Akçelik M3D).

HV (%) values are calculated for All Movement Classes of All Heavy Vehicle Model Designation.

Arrival Flows used in performance calculations are adjusted to include any Initial Queued Demand and Upstream Capacity Constraint effects.

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| Int Delay, s/veh | 3.2 | | | | | | |
|------------------------|------|------|------|------|------|------|--|
| Movement | EBL | EBR | NBL | NBT | SBT | SBR | |
| Lane Configurations | ľ | 1 | ľ | 1 | 4 | | |
| Traffic Vol, veh/h | 105 | 36 | 25 | 278 | 595 | 100 | |
| Future Vol, veh/h | 105 | 36 | 25 | 278 | 595 | 100 | |
| Conflicting Peds, #/hr | 0 | 0 | 0 | 0 | 0 | 0 | |
| Sign Control | Stop | Stop | Free | Free | Free | Free | |
| RT Channelized | - | None | - | None | - | None | |
| Storage Length | 100 | 0 | 80 | - | - | - | |
| Veh in Median Storage | ,# 0 | - | - | 0 | 0 | - | |
| Grade, % | 0 | - | - | 0 | 0 | - | |
| Peak Hour Factor | 98 | 98 | 98 | 98 | 98 | 98 | |
| Heavy Vehicles, % | 3 | 3 | 9 | 5 | 3 | 1 | |
| Mvmt Flow | 107 | 37 | 26 | 284 | 607 | 102 | |

| Major/Minor | Minor2 | l | Major1 | Maj | or2 | | |
|----------------------|--------|-------|--------|-----|-----|---|--|
| Conflicting Flow All | 993 | 658 | 709 | 0 | - | 0 | |
| Stage 1 | 658 | - | - | - | - | - | |
| Stage 2 | 335 | - | - | - | - | - | |
| Critical Hdwy | 6.43 | 6.23 | 4.19 | - | - | - | |
| Critical Hdwy Stg 1 | 5.43 | - | - | - | - | - | |
| Critical Hdwy Stg 2 | 5.43 | - | - | - | - | - | |
| Follow-up Hdwy | 3.527 | 3.327 | 2.281 | - | - | - | |
| Pot Cap-1 Maneuver | 271 | 462 | 858 | - | - | - | |
| Stage 1 | 513 | - | - | - | - | - | |
| Stage 2 | 723 | - | - | - | - | - | |
| Platoon blocked, % | | | | - | - | - | |
| Mov Cap-1 Maneuver | 263 | 462 | 858 | - | - | - | |
| Mov Cap-2 Maneuver | 263 | - | - | - | - | - | |
| Stage 1 | 498 | - | - | - | - | - | |
| Stage 2 | 723 | - | - | - | - | - | |
| | | | | | | | |
| | | | | | | | |

| Approach | EB | NB | SB | |
|--------------------|------------|------|----|--|
| HCM Control Delay, | , s/v24.13 | 0.77 | 0 | |
| HCM LOS | С | | | |

| Minor Lane/Major Mvmt | NBL | NBT EBLn1 | EBLn2 | SBT | SBR | |
|---------------------------|------|-----------|-------|-----|-----|--|
| Capacity (veh/h) | 858 | - 263 | 462 | - | - | |
| HCM Lane V/C Ratio | 0.03 | - 0.407 | 0.079 | - | - | |
| HCM Control Delay (s/veh) | 9.3 | - 27.8 | 13.5 | - | - | |
| HCM Lane LOS | А | - D | В | - | - | |
| HCM 95th %tile Q(veh) | 0.1 | - 1.9 | 0.3 | - | - | |

| Movement EBL EBR NBL NBT SBT SBR Lane Configurations 1 | Int Delay, s/veh | 1.7 | | | | | | | |
|--|------------------------|----------|------|------|------|--------------|------|--|--|
| Lane Configurations Image: Configuration in the image: Configuration | Movement | EBL | EBR | NBL | NBT | SBT | SBR | | |
| Traffic Vol, veh/h 55 27 15 260 566 73 Future Vol, veh/h 55 27 15 260 566 73 Conflicting Peds, #/hr 0 0 0 0 0 0 Sign Control Stop Stop Free Free Free Free RT Channelized - None - None - None Storage Length 100 0 115 - - Veh in Median Storage, # 0 - - 0 0 Grade, % 0 - - 0 0 - Peak Hour Factor 92 92 92 92 92 92 Heavy Vehicles, % 1 9 1 6 3 1 Mvmt Flow 60 29 16 283 615 79 | Lane Configurations | <u>۲</u> | 1 | - ኘ | ↑ | - 1 2 | | | |
| Future Vol, veh/h 55 27 15 260 566 73 Conflicting Peds, #/hr 0 0 0 0 0 0 Sign Control Stop Stop Free Free Free Free RT Channelized - None - None - None Storage Length 100 0 115 - - - Veh in Median Storage, # 0 - - 0 0 - Grade, % 0 - - 0 0 - Peak Hour Factor 92 92 92 92 92 92 Heavy Vehicles, % 1 9 1 6 3 1 Mvmt Flow 60 29 16 283 615 79 | Traffic Vol, veh/h | 55 | 27 | 15 | 260 | 566 | 73 | | |
| Conflicting Peds, #/hr 0 115 - <td>Future Vol, veh/h</td> <td>55</td> <td>27</td> <td>15</td> <td>260</td> <td>566</td> <td>73</td> <td></td> <td></td> | Future Vol, veh/h | 55 | 27 | 15 | 260 | 566 | 73 | | |
| Sign ControlStopStopFreeFreeFreeFreeFreeRT Channelized-None-None-NoneStorage Length1000115Veh in Median Storage, #000-Grade, %000-Peak Hour Factor9292929292Heavy Vehicles, %191631Mvmt Flow60291628361579 | Conflicting Peds, #/hr | 0 | 0 | 0 | 0 | 0 | 0 | | |
| RT Channelized - None - None Storage Length 100 0 115 - - Veh in Median Storage, # 0 - - 0 0 Grade, % 0 - - 0 0 - Peak Hour Factor 92 92 92 92 92 Heavy Vehicles, % 1 9 1 6 3 1 Mvmt Flow 60 29 16 283 615 79 | Sign Control | Stop | Stop | Free | Free | Free | Free | | |
| Storage Length 100 0 115 - 0 0 - - - - 0 0 - - - 0 0 - - 0 0 - - 0 0 - - 0 0 - 0 0 - 0 0 - 0 1 0 1 0 1 0 1 0 1 0 1 0 1 0 | RT Channelized | - | None | - | None | - | None | | |
| Veh in Median Storage, # 0 - 0 0 - Grade, % 0 - - 0 0 - Peak Hour Factor 92 92 92 92 92 92 Heavy Vehicles, % 1 9 1 6 3 1 Mvmt Flow 60 29 16 283 615 79 | Storage Length | 100 | 0 | 115 | - | - | - | | |
| Grade, % 0 - 0 0 - Peak Hour Factor 92 92 92 92 92 Heavy Vehicles, % 1 9 1 6 3 1 Mvmt Flow 60 29 16 283 615 79 | Veh in Median Storage | ,# 0 | - | - | 0 | 0 | - | | |
| Peak Hour Factor 92 92 92 92 92 Heavy Vehicles, % 1 9 1 6 3 1 Mvmt Flow 60 29 16 283 615 79 | Grade, % | 0 | - | - | 0 | 0 | - | | |
| Heavy Vehicles, % 1 9 1 6 3 1 Mvmt Flow 60 29 16 283 615 79 | Peak Hour Factor | 92 | 92 | 92 | 92 | 92 | 92 | | |
| Mvmt Flow 60 29 16 283 615 79 | Heavy Vehicles, % | 1 | 9 | 1 | 6 | 3 | 1 | | |
| | Mvmt Flow | 60 | 29 | 16 | 283 | 615 | 79 | | |

| Major/Minor | Minor2 | l | Major1 | Ma | jor2 | |
|----------------------|--------|-------|--------|----|------|---|
| Conflicting Flow All | 970 | 655 | 695 | 0 | - | 0 |
| Stage 1 | 655 | - | - | - | - | - |
| Stage 2 | 315 | - | - | - | - | - |
| Critical Hdwy | 6.41 | 6.29 | 4.11 | - | - | - |
| Critical Hdwy Stg 1 | 5.41 | - | - | - | - | - |
| Critical Hdwy Stg 2 | 5.41 | - | - | - | - | - |
| Follow-up Hdwy | 3.509 | 3.381 | 2.209 | - | - | - |
| Pot Cap-1 Maneuver | 282 | 454 | 906 | - | - | - |
| Stage 1 | 519 | - | - | - | - | - |
| Stage 2 | 742 | - | - | - | - | - |
| Platoon blocked, % | | | | - | - | - |
| Mov Cap-1 Maneuver | 277 | 454 | 906 | - | - | - |
| Mov Cap-2 Maneuver | 277 | - | - | - | - | - |
| Stage 1 | 509 | - | - | - | - | - |
| Stage 2 | 742 | - | - | - | - | - |
| | | | | | | |

| Approach | EB | NB | SB |
|-------------------|------------|------|----|
| HCM Control Delay | , s/v18.89 | 0.49 | 0 |
| HCM LOS | С | | |

| Minor Lane/Major Mvmt | NBL | NBT EBLn1 | EBLn2 | SBT | SBR | |
|---------------------------|-------|-----------|-------|-----|-----|--|
| Capacity (veh/h) | 906 | - 277 | 454 | - | - | |
| HCM Lane V/C Ratio | 0.018 | - 0.216 | 0.065 | - | - | |
| HCM Control Delay (s/veh) | 9 | - 21.5 | 13.5 | - | - | |
| HCM Lane LOS | А | - C | В | - | - | |
| HCM 95th %tile Q(veh) | 0.1 | - 0.8 | 0.2 | - | - | |

Int Delay s/yeh

| Int Delay, s/veh | 3.5 | | | | | | |
|------------------------|--------|------|------|------|------|------|---|
| Movement | WBL | WBR | NBT | NBR | SBL | SBT | - |
| Lane Configurations | ۰¥ | | 4 | | | ्स | • |
| Traffic Vol, veh/h | 35 | 96 | 179 | 65 | 154 | 441 | |
| Future Vol, veh/h | 35 | 96 | 179 | 65 | 154 | 441 | |
| Conflicting Peds, #/hr | 0 | 0 | 0 | 0 | 0 | 0 |) |
| Sign Control | Stop | Stop | Free | Free | Free | Free | ; |
| RT Channelized | - | None | - | None | - | None | ; |
| Storage Length | 0 | - | - | - | - | - | - |
| Veh in Median Storage | e, # 0 | - | 0 | - | - | 0 |) |
| Grade, % | 0 | - | 0 | - | - | 0 |) |
| Peak Hour Factor | 94 | 94 | 94 | 94 | 94 | 94 | ŀ |
| Heavy Vehicles, % | 4 | 9 | 4 | 1 | 4 | 3 | 3 |
| Mvmt Flow | 37 | 102 | 190 | 69 | 164 | 469 |) |

| Major/Minor | Minor1 | Ν | lajor1 | Ν | lajor2 | |
|----------------------|--------|-------|--------|---|--------|---|
| Conflicting Flow All | 1022 | 225 | 0 | 0 | 260 | 0 |
| Stage 1 | 225 | - | - | - | - | - |
| Stage 2 | 797 | - | - | - | - | - |
| Critical Hdwy | 6.44 | 6.29 | - | - | 4.14 | - |
| Critical Hdwy Stg 1 | 5.44 | - | - | - | - | - |
| Critical Hdwy Stg 2 | 5.44 | - | - | - | - | - |
| Follow-up Hdwy | 3.536 | 3.381 | - | - | 2.236 | - |
| Pot Cap-1 Maneuver | 259 | 797 | - | - | 1293 | - |
| Stage 1 | 808 | - | - | - | - | - |
| Stage 2 | 440 | - | - | - | - | - |
| Platoon blocked, % | | | - | - | | - |
| Mov Cap-1 Maneuver | 215 | 797 | - | - | 1293 | - |
| Mov Cap-2 Maneuver | 215 | - | - | - | - | - |
| Stage 1 | 808 | - | - | - | - | - |
| Stage 2 | 365 | - | - | - | - | - |
| | | | | | | |

| Approach | VB | NB | SB |
|--------------------------|----|----|------|
| HCM Control Delay, s/v16 | 11 | 0 | 2.12 |
| HCMLOS | С | | |

| Minor Lane/Major Mvmt | NBT | NBRWBLn | SBL | SBT | |
|---------------------------|-----|---------|--------|-----|--|
| Capacity (veh/h) | - | - 462 | 2 1293 | - | |
| HCM Lane V/C Ratio | - | - 0.30 | 0.127 | - | |
| HCM Control Delay (s/veh) | - | - 16.1 | 8.2 | 0 | |
| HCM Lane LOS | - | - (|) А | Α | |
| HCM 95th %tile Q(veh) | - | - 1.3 | 8 0.4 | - | |

Intersection Delay, s/veh Intersection LOS

13.8

В

| Movement | EBL | EBT | EBR | WBL | WBT | WBR | NBL | NBT | NBR | SBL | SBT | SBR |
|----------------------------|------|------|------|------|------|------|------|------|------|------|------|------|
| Lane Configurations | | 4 | | | 4 | | | 4 | | | 4 | |
| Traffic Vol, veh/h | 37 | 16 | 21 | 6 | 61 | 234 | 2 | 4 | 0 | 239 | 139 | 80 |
| Future Vol, veh/h | 37 | 16 | 21 | 6 | 61 | 234 | 2 | 4 | 0 | 239 | 139 | 80 |
| Peak Hour Factor | 0.97 | 0.97 | 0.97 | 0.97 | 0.97 | 0.97 | 0.97 | 0.97 | 0.97 | 0.97 | 0.97 | 0.97 |
| Heavy Vehicles, % | 3 | 20 | 1 | 1 | 2 | 3 | 1 | 25 | 1 | 2 | 1 | 8 |
| Mvmt Flow | 38 | 16 | 22 | 6 | 63 | 241 | 2 | 4 | 0 | 246 | 143 | 82 |
| Number of Lanes | 0 | 1 | 0 | 0 | 1 | 0 | 0 | 1 | 0 | 0 | 1 | 0 |
| Approach | EB | | | WB | | | NB | | | SB | | |
| Opposing Approach | WB | | | EB | | | SB | | | NB | | |
| Opposing Lanes | 1 | | | 1 | | | 1 | | | 1 | | |
| Conflicting Approach Left | SB | | | NB | | | EB | | | WB | | |
| Conflicting Lanes Left | 1 | | | 1 | | | 1 | | | 1 | | |
| Conflicting Approach Right | NB | | | SB | | | WB | | | EB | | |
| Conflicting Lanes Right | 1 | | | 1 | | | 1 | | | 1 | | |
| HCM Control Delay, s/veh | 9.4 | | | 11.2 | | | 8.8 | | | 16.2 | | |
| HCM LOS | А | | | В | | | А | | | С | | |

| Lane | NBLn1 | EBLn1 | WBLn1 | SBLn1 |
|--------------------------|-------|-------|-------|-------|
| Vol Left, % | 33% | 50% | 2% | 52% |
| Vol Thru, % | 67% | 22% | 20% | 30% |
| Vol Right, % | 0% | 28% | 78% | 17% |
| Sign Control | Stop | Stop | Stop | Stop |
| Traffic Vol by Lane | 6 | 74 | 301 | 458 |
| LT Vol | 2 | 37 | 6 | 239 |
| Through Vol | 4 | 16 | 61 | 139 |
| RT Vol | 0 | 21 | 234 | 80 |
| Lane Flow Rate | 6 | 76 | 310 | 472 |
| Geometry Grp | 1 | 1 | 1 | 1 |
| Degree of Util (X) | 0.01 | 0.119 | 0.41 | 0.637 |
| Departure Headway (Hd) | 5.689 | 5.604 | 4.762 | 4.859 |
| Convergence, Y/N | Yes | Yes | Yes | Yes |
| Сар | 632 | 644 | 748 | 737 |
| Service Time | 3.696 | 3.604 | 2.846 | 2.948 |
| HCM Lane V/C Ratio | 0.009 | 0.118 | 0.414 | 0.64 |
| HCM Control Delay, s/veh | 8.8 | 9.4 | 11.2 | 16.2 |
| HCM Lane LOS | А | А | В | С |
| HCM 95th-tile Q | 0 | 0.4 | 2 | 4.6 |

₩ Site: 7 [3. E Scott Ave & Lewis River Road (Site Folder: Forecast 2026 With Project)]

Output produced by SIDRA INTERSECTION Version: 9.1.3.210

Forecast 2028 PM Peak Hour With Project Site Category: (None) Roundabout

| Vehic | le Mo | ovement | Perfor | man | ce | | | | | | | | | | |
|-----------|---------|--------------|------------------------------|---------------------------|------------------------------|----------------------------|---------------------|-----------------------|---------------------|----------------------------|---------------------------------|--------------|----------------------|---------------------------|-----------------------|
| Mov ID | Turn | Mov Class | Dem F [Total veh/h | nand lows HV] % | Ar Fl [Total veh/h | rival lows HV] % | Deg. Satn v/c | Aver. Delay sec | Level of Service | 95% Qi [Veh. veh | Back Of ueue Dist] ft | Prop. Que | Eff. Stop Rate | Aver. No. of Cycles | Aver. Speed mph |
| South | Lewi | s River R | oad | | | | | | | | | | | | |
| 3 | L2 | All MCs | 101 | 1.6 | 101 | 1.6 | 0.764 | 14.3 | LOS B | 10.4 | 262.2 | 0.85 | 0.70 | 0.97 | 33.5 |
| 18a | R1 | All MCs | 779 | 1.0 | 779 | 1.0 | 0.764 | 7.6 | LOS A | 10.4 | 262.2 | 0.85 | 0.70 | 0.97 | 34.2 |
| Appro | ach | | 880 | 1.1 | 880 | 1.1 | 0.764 | 8.3 | LOS A | 10.4 | 262.2 | 0.85 | 0.70 | 0.97 | 34.1 |
| NorthE | East: L | ewis Rive | er Road | | | | | | | | | | | | |
| 1ax | L1 | All MCs | 407 | 1.2 | 407 | 1.2 | 0.436 | 9.2 | LOS A | 3.5 | 89.5 | 0.40 | 0.54 | 0.40 | 33.4 |
| 16ax | R1 | All MCs | 165 | 1.0 | 165 | 1.0 | 0.436 | 3.8 | LOS A | 3.5 | 89.5 | 0.40 | 0.54 | 0.40 | 34.2 |
| Appro | ach | | 572 | 1.1 | 572 | 1.1 | 0.436 | 7.7 | LOS A | 3.5 | 89.5 | 0.40 | 0.54 | 0.40 | 33.7 |
| West: | E Sco | ott Avenue | 9 | | | | | | | | | | | | |
| 5a | L1 | All MCs | 271 | 1.0 | 271 | 1.0 | 0.289 | 10.9 | LOS B | 1.8 | 46.4 | 0.61 | 0.66 | 0.61 | 32.5 |
| 12 | R2 | All MCs | 28 | 1.0 | 28 | 1.0 | 0.289 | 6.0 | LOS A | 1.8 | 46.4 | 0.61 | 0.66 | 0.61 | 32.9 |
| Appro | ach | | 299 | 1.0 | 299 | 1.0 | 0.289 | 10.4 | LOS B | 1.8 | 46.4 | 0.61 | 0.66 | 0.61 | 32.5 |
| All Vel | nicles | | 1751 | 1.1 | 1751 | 1.1 | 0.764 | 8.5 | LOS A | 10.4 | 262.2 | 0.66 | 0.64 | 0.72 | 33.7 |

Site Level of Service (LOS) Method: Delay & Degree of Saturation (SIDRA). Site LOS Method is specified in the Parameter Settings dialog (Options tab).

Roundabout LOS Method: Same as Signalised Intersections.

Vehicle movement LOS values are based on average delay and v/c ratio (degree of saturation) per movement.

Intersection and Approach LOS values are based on average delay for all movements (v/c not used).

Roundabout Capacity Model: SIDRA HCM.

Delay Model: SIDRA Standard (Control Delay: Geometric Delay is included).

Queue Model: SIDRA queue estimation methods are used for Back of Queue and Queue at Start of Gap.

Gap-Acceptance Capacity Formula: SIDRA Standard (Akçelik M3D).

HV (%) values are calculated for All Movement Classes of All Heavy Vehicle Model Designation.

Arrival Flows used in performance calculations are adjusted to include any Initial Queued Demand and Upstream Capacity Constraint effects.

SIDRA INTERSECTION 9.1 | Copyright © 2000-2023 Akcelik and Associates Pty Ltd | sidrasolutions.com Organisation: HEATH & ASSOCIATES | Licence: PLUS / 1PC | Processed: Tuesday, July 25, 2023 4:01:18 PM Project: C:\Users\pwhalen\Heath and Associates\Traffic Studies - Documents\Sidra\5183\3. Forecast 2026 With Project.sip9

| Int Delay, s/veh | 1.5 | | | | | | | |
|------------------------|------|------|------|------|--------------|------|--|--|
| Movement | EBL | EBR | NBL | NBT | SBT | SBR | | |
| Lane Configurations | ۰Y | | | ୍ କ | - 1 2 | | | |
| Traffic Vol, veh/h | 29 | 36 | 27 | 238 | 432 | 32 | | |
| Future Vol, veh/h | 29 | 36 | 27 | 238 | 432 | 32 | | |
| Conflicting Peds, #/hr | 0 | 0 | 0 | 0 | 0 | 0 | | |
| Sign Control | Stop | Stop | Free | Free | Free | Free | | |
| RT Channelized | - | None | - | None | - | None | | |
| Storage Length | - | - | - | - | - | - | | |
| Veh in Median Storage | ,# 0 | - | - | 0 | 0 | - | | |
| Grade, % | 0 | - | - | 0 | 0 | - | | |
| Peak Hour Factor | 92 | 92 | 92 | 92 | 92 | 92 | | |
| Heavy Vehicles, % | 2 | 2 | 2 | 2 | 3 | 2 | | |
| Mvmt Flow | 32 | 39 | 29 | 259 | 470 | 35 | | |

| Major/Minor | Minor2 | Major1 Major2 | | | | |
|----------------------|--------|---------------|-------|---|---|---|
| Conflicting Flow All | 804 | 487 | 504 | 0 | - | 0 |
| Stage 1 | 487 | - | - | - | - | - |
| Stage 2 | 317 | - | - | - | - | - |
| Critical Hdwy | 6.42 | 6.22 | 4.12 | - | - | - |
| Critical Hdwy Stg 1 | 5.42 | - | - | - | - | - |
| Critical Hdwy Stg 2 | 5.42 | - | - | - | - | - |
| Follow-up Hdwy | 3.518 | 3.318 | 2.218 | - | - | - |
| Pot Cap-1 Maneuver | 352 | 581 | 1060 | - | - | - |
| Stage 1 | 618 | - | - | - | - | - |
| Stage 2 | 738 | - | - | - | - | - |
| Platoon blocked, % | | | | - | - | - |
| Mov Cap-1 Maneuver | 341 | 581 | 1060 | - | - | - |
| Mov Cap-2 Maneuver | 341 | - | - | - | - | - |
| Stage 1 | 598 | - | - | - | - | - |
| Stage 2 | 738 | - | - | - | - | - |
| | | | | | | |
| | | | | | | |

| Approach | EB | NB | SB | |
|----------------------|----------|------|----|--|
| HCM Control Delay, s | s/v14.69 | 0.87 | 0 | |
| HCM LOS | В | | | |

| Minor Lane/Major Mvmt | NBL | NBT E | BLn1 | SBT | SBR |
|---------------------------|-------|-------|------|-----|-----|
| Capacity (veh/h) | 1060 | - | 442 | - | - |
| HCM Lane V/C Ratio | 0.028 | - | 0.16 | - | - |
| HCM Control Delay (s/veh) | 8.5 | 0 | 14.7 | - | - |
| HCM Lane LOS | A | A | В | - | - |
| HCM 95th %tile Q(veh) | 0.1 | - | 0.6 | - | - |



Exhibit 1310-7 Left-Turn Storage Guidelines: Two-Lane, Unsignalized